



Technische  
Universität  
Braunschweig



## **A parametric ROM for the linear frequency domain approach to time-accurate CFD**

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Model Reduction of Complex Dynamical Systems

ModRed, MPI Magdeburg Dec. 11-13

# A parametric ROM for the LFD approach to CFD

- **Motivation: Parametric reduced-order models**
- Interpolating data on manifolds
- The Linear Frequency Domain (LFD) approach to CFD
- Offline, semi-offline and online ROM stages
- A practical example
- Conclusions & Outlook

## Motivation: Parametric reduced-order models

### Key idea of subspace based reduced order modeling:

- Construct **low-dimensional** subspace
- Restrict computations to **low-dimensional** subspace (e.g. via projection)

### Examples:

- Reduced Bases methods
- Krylov subspace methods
- Proper Orthogonal Decomposition

# Motivation: Parametric reduced-order models

In this talk:

Parameter dependent large-scale linear systems:

$$A(p, q)W = b(p, q), \quad A \in \mathbb{R}^{n \times n}, \quad b \in \mathbb{R}^n$$

- Parameters  $q$  determine operating points
- Parameters  $p$  are considered as examination parameters

## Motivation: Parametric reduced-order models

**Standard order reduction ansatz:** use subspace of dim  $m \ll n$

$$W(p, q_0) = U_{q_0} a(p), \quad U_{q_0} \in \mathbb{R}^{n \times m}$$

Determine coefficient vector  $a(p) \in \mathbb{R}^m$  via

- **Orthogonal residual condition**

$$U_{q_0}^T S A U_{q_0} a = U_{q_0}^T S b \in \mathbb{R}^m$$

- **Minimum residual condition**

$$U_{q_0}^T A^T S A U_{q_0} a = U_{q_0}^T A^T S b \in \mathbb{R}^m$$

inner product:  $\langle \cdot, \cdot \rangle = (\cdot)^T S (\cdot)$

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$$U_{q_0}^T S A U_{q_0} a = U_{q_0}^T S b \in \mathbb{R}^m$$

$$A_{orth} a = b_{orth}$$

- **Minimum residual condition**

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$$A_{\min} a = b_{\min}$$



## Motivation: Parametric reduced-order models

- Suppose that at  $r$  operating points, we have computed bases

$$U_{q_1}, \dots, U_{q_r}$$

- Objective: Construct ROM at new operating point

$$W(p, q_*) = U_{q_*} a(p), \quad U_{q_*} \in \mathbb{R}^{n \times m}$$

- Required: Parametrized **trajectory** of projection bases

$$U: q \mapsto U_q$$

- Idea: **Interpolate** given bases [1] [2]

[1] D. Amsallem, C. Farhat, 2008

[2] Nguyen T.S., 2012



## Motivation: Parametric reduced-order models

### Challenges:

- ROM subspace spanned by orthogonal reduced-order basis (ROB)
- Ensure that parametric variation always gives orthogonal bases

Reduced bases matrices **must** be considered as points in the Grassmann manifold of  $k$ -dimensional subspaces or the Stiefel manifold of “tall-skinny” orthonormal matrices<sup>[3]</sup>

[3] A. Edelman, T.A. Arias, S.T. Smith, 1998

# A parametric ROM for the LFD approach to CFD

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# Interpolating data on manifolds (A): basic principle

## Matrix manifolds

- **Stiefel manifold**

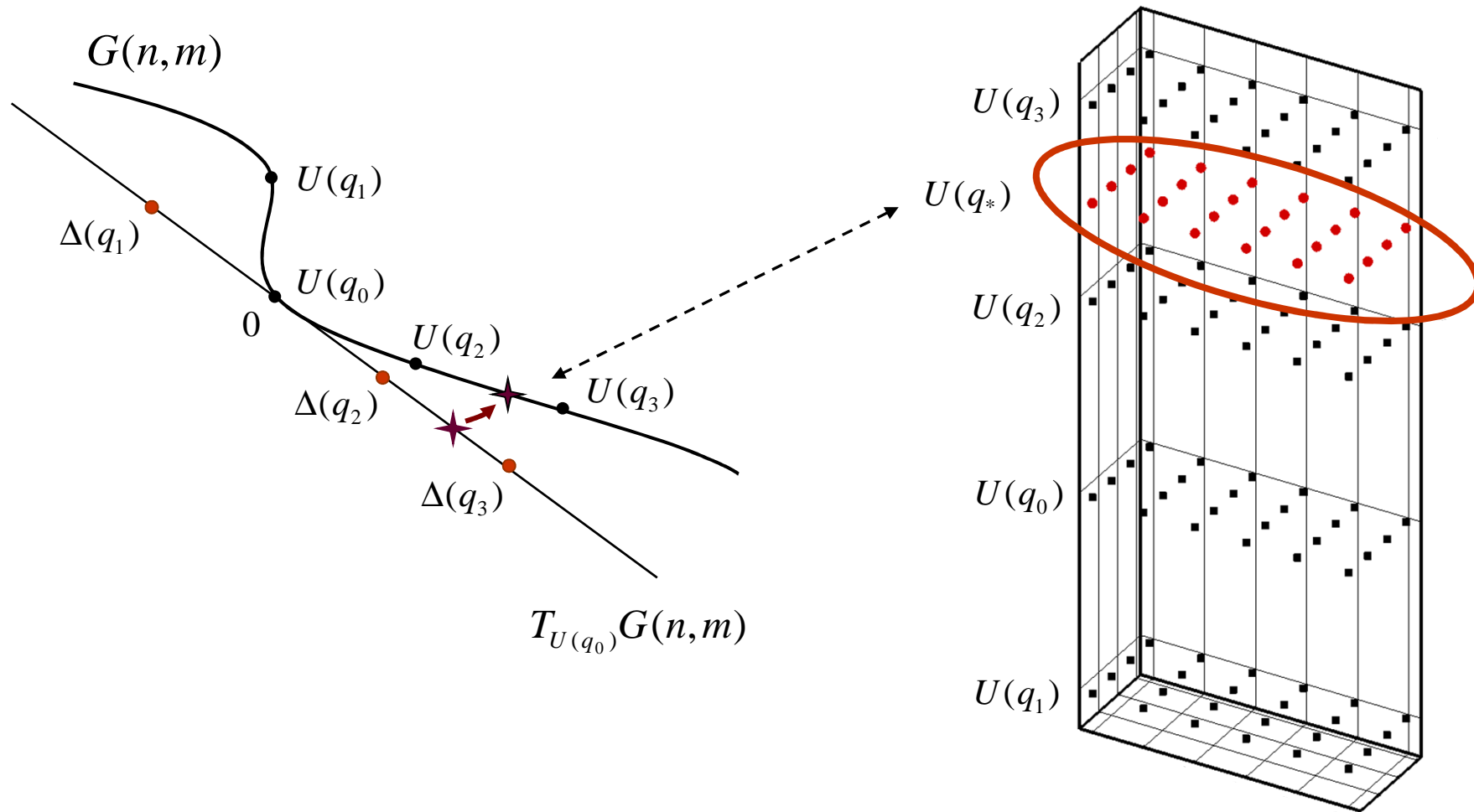
$$V(n, m) = \{Y \in \mathbb{R}^{n \times m} \mid Y^T Y = I_{m \times m}\}$$

- **Grassmann manifold**

$$G(n, m) = \{S \leq \mathbb{R}^n \mid \dim(S) = m\}$$

=> each point is a subspace of dimension  $m$ ,  
equivalence class of matrices spanning a given subspace may  
be represented by point in Stiefel manifold

# Interpolating data on manifolds (A): basic principle



# Interpolating data on manifolds (B): Matrix Manifolds

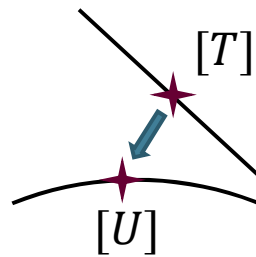
...and here numerical linear algebra comes in

- Grassmann exponential mapping

$$[T] \in T_{[U_0]} G(n, m), \quad U_0^T T = 0_{m \times m} :$$

$$\exp_{[U_0]}([T]) = [U_0 Q \cos(\Sigma) + W \sin(\Sigma)] \in G(n, m),$$

$$W \Sigma Q^T \underset{SVD}{=} T$$

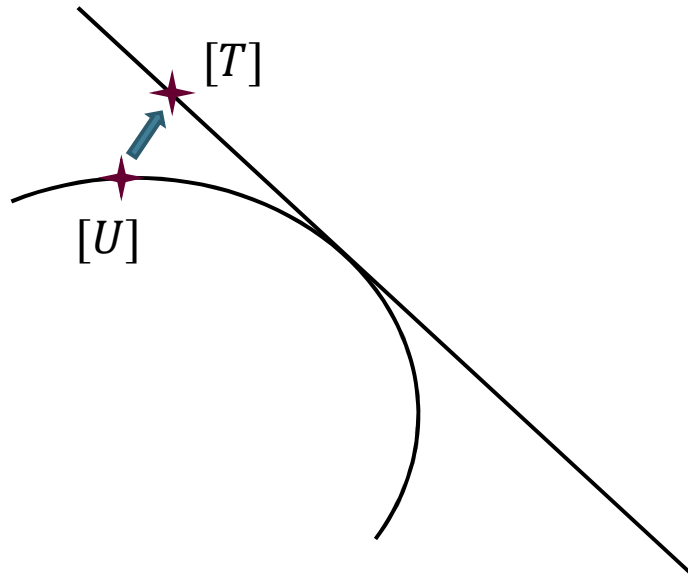


Isometric mapping: tangent space to manifold

# Interpolating data on manifolds (B): Matrix Manifolds

...and here numerical linear algebra comes in

- Grassmann logarithmic mapping



$$[U] \in G(n, m), \quad U^T U = I_{m \times m} :$$

$$\log_{[U_0]}([U]) = [T] \in T_{[U_0]}G(n, m),$$

$$T = W \tan^{-1}(\Sigma),$$

$$W \Sigma Q^T \underset{SVD}{=} (I_{n \times n} - U_0 U_0^T) U (U^T U_0)^{-1}$$

Isometric mapping: manifold to tangent space

# Interpolating data on manifolds (C): A word of caution

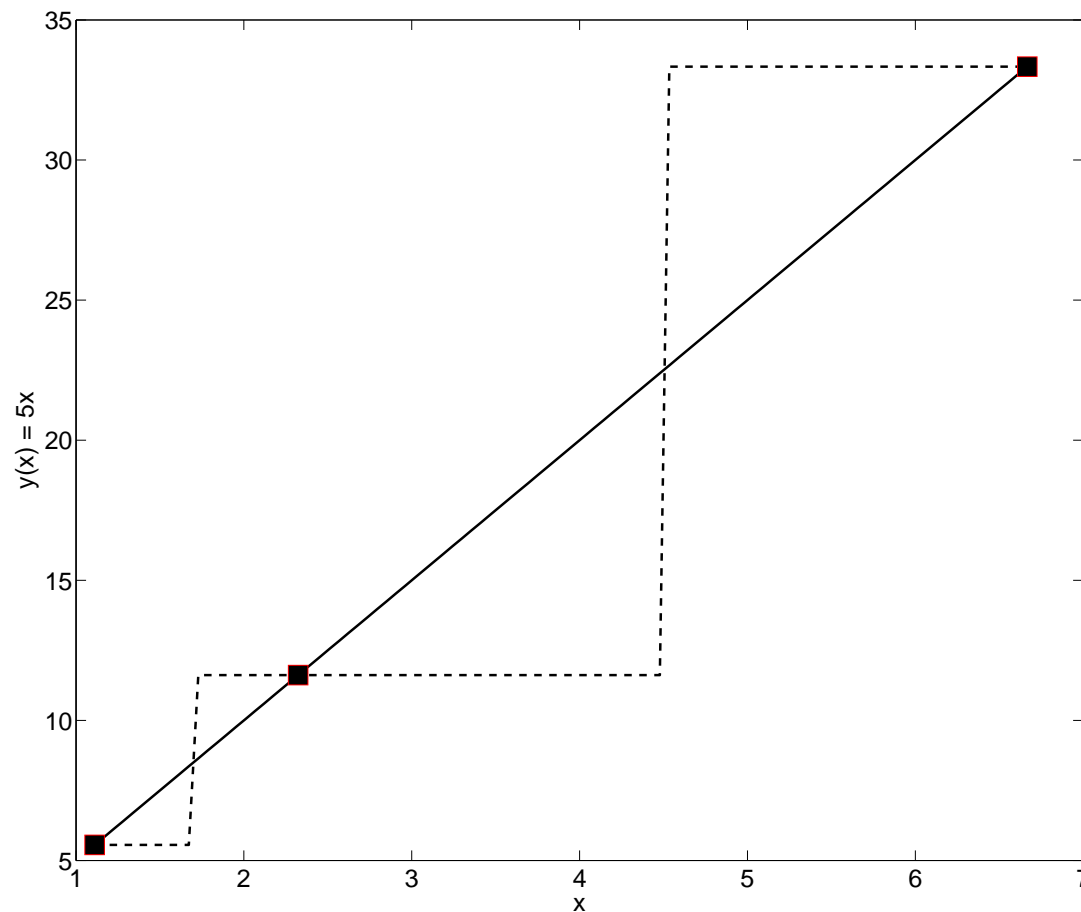
## Challenges

- It cannot be taken for granted that the interpolation's result stays in the tangential space!
  - There are interpolation schemes, that are not admissible in this regard!
- Tangential vectors are represented by  $(n \times m)$ -matrices:
  - Entry-by-entry interpolation may require millions of interpolation procedures

# Interpolating data on manifolds (C): A word of caution

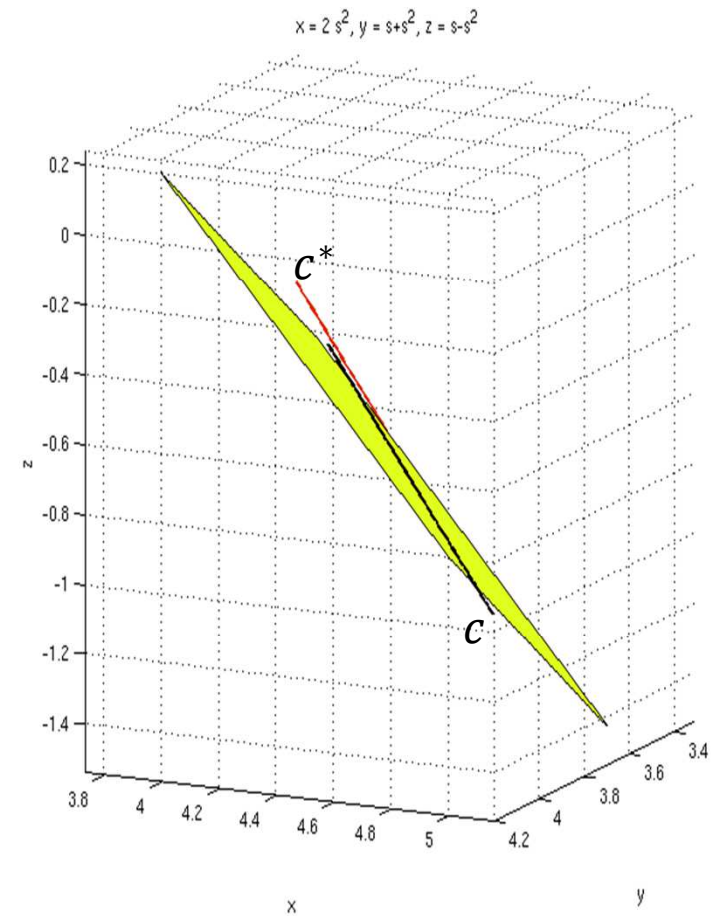
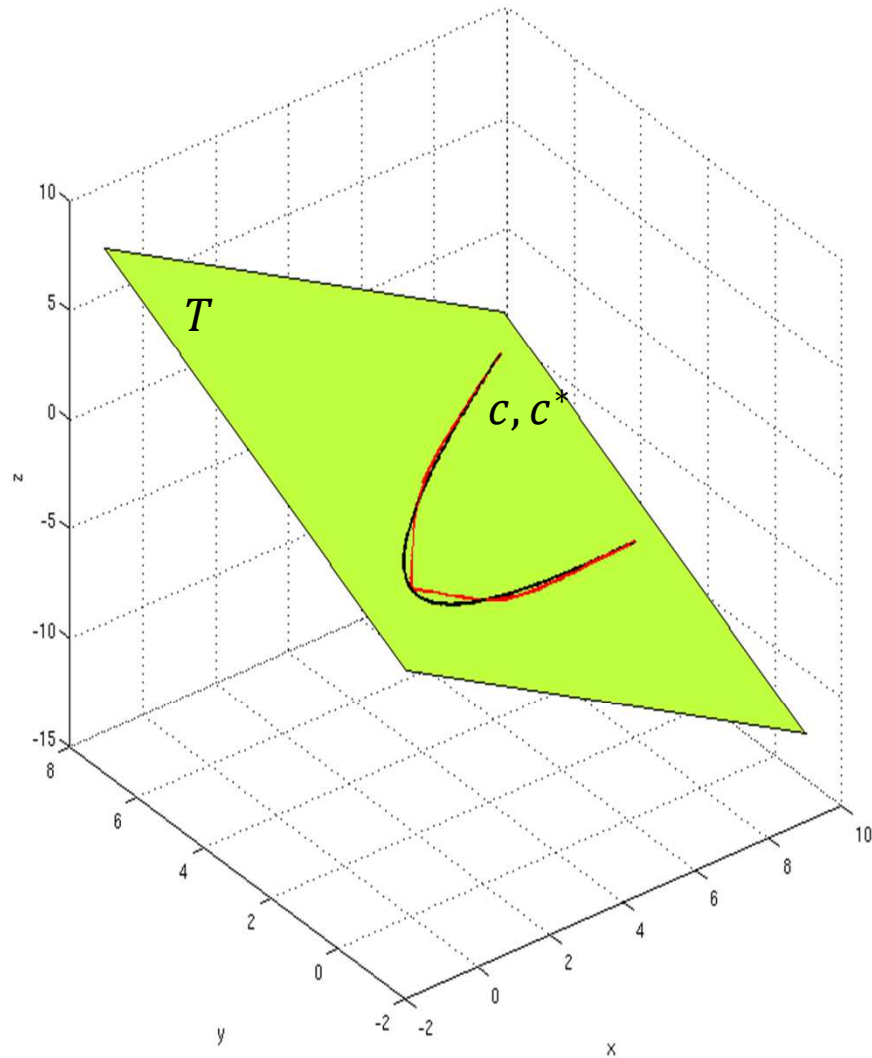
Trivial example:

Nearest-neighbor  
interpolation  
leaves the data  
subspace





# Interpolating data on manifolds (C): A word of caution



# Interpolating data on manifolds (C): A word of caution

## Conclusion

- Let  $T^1 = T(q_1), \dots, T^k = T(q_k)$  be vectors in a Grassmann tangent space, represented by  $n \times m$  – matrices
- An admissible interpolator must be of the form

$$T^*(q) = \sum_{l=1}^k f_l(q) T^l$$

- In 1D, e.g. **linear** interpolation and **Lagrange** interpolation fulfill this requirement
- In multiple D, **radial basis function** interpolation is feasible

# A parametric ROM for the LFD approach to CFD

- Motivation: Parametric reduced-order models
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- Offline, semi-offline and online ROM stages
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- Conclusions & Outlook

# The linear frequency approach to CFD

## Underlying assumption

- Flow to be simulated is **periodic** and approximately **harmonic**
  - Valid for pitching motions of small amplitude



- Flow state vector given by **mean flow + time-dependent fluctuations**

$$W(t) = \bar{W} + \tilde{W}(t) \in \mathbb{R}^N, \quad N = \#(\text{flow vars}) \#(\text{grid points})$$

- Same applies to **grid coordinates** and **grid cell volumes**

## The linear frequency approach to CFD

First-order Taylor and transition to Fourier space give complex linear system:

$$(DR_W + i\omega\bar{M})\hat{W} = b_1 + i\omega b_2 \in \mathbb{C}^N$$

( $\bar{M}$  = temporal mean of grid cell volumes,  $\omega$  = frequency)

# The linear frequency approach to CFD

First-order Taylor and transition to Fourier space give complex linear system:

$$(DR_W + i\omega\bar{M})\hat{W} = b_1 + i\omega b_2 \in \mathbb{C}^N$$

$$A(\omega, Ma)\hat{W} = b(\omega, Ma) \in \mathbb{C}^N$$

( $\bar{M}$  = temporal mean of grid cell volumes,  $\omega$  = frequency)

**Parametric dependency:**

- Mach number determines operating point (mean value)  $q = Ma$
- Frequency varies at each operating point  $p = \omega$

$$\hat{W} = \hat{W}(\omega, Ma) \in \mathbb{C}^N$$

# A parametric ROM for the LFD approach to CFD

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# Offline, semi-offline and online stage

## Offline stage

- Select operating points (**OPs**)  $q_1, \dots, q_r$
- At each **OP**, compute projection basis  $U_{q_k}$  via **snapshot POD**



## Offline, semi-offline and online stage

### Offline stage

- Select operating points (**OPs**)  $q_1, \dots, q_r$
- At each **OP**, compute projection basis  $U_{q_k}$  via **snapshot POD**
- For any **OP**  $q_*$  of interest, assess the trajectory

$$U: q \mapsto U_q$$

via Grassmann Interpolation to obtain  $U_{q_*} = U(q_*) \in \mathbb{C}^{N \times m}$

## Offline, semi-offline and online stage

### Semi-offline stage

- At operating point  $q_*$ , project full order system onto  $U_{q_*}$
- Exploit **separable** parameter dependency:

$$\begin{aligned} A_{min}(\omega, q_*) &= U_{q_*}^T (DR_W + i\omega\bar{M})^T S (DR_W + i\omega\bar{M}) U_{q_*} \\ &= E(q_*) + \omega^2 G(q_*) + i\omega H(q_*) \in \mathbb{C}^{m \times m} \end{aligned}$$

$$\begin{aligned} b_{min}(\omega, q_*) &= \beta_{min,1}(q_*) + \omega^2 \beta_{min,2}(q_*) + i\omega \beta_{min,3}(q_*) \in \mathbb{C}^m \end{aligned}$$



## Offline, semi-offline and online stage

### Semi-offline stage

- At operating point  $q_*$ , project full order system onto  $U_{q_*}$
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Similar for **orth res** approach

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## Offline, semi-offline and online stage

### Semi-offline stage

- At operating point  $q_*$ , project full order system onto  $U_{q_*}$
- Exploit **separable** parameter dependency: precompute

$$E(q_*), \quad G(q_*), \quad H(q_*) \in \mathbb{C}^{m \times m}$$

$$\beta_{min,1}(q_*), \quad \beta_{min,2}(q_*), \quad \beta_{min,3}(q_*) \in \mathbb{C}^m$$

## Offline, semi-offline and online stage

### Online stage

- For any frequency  $\omega$  compute reduced system and right hand side

$$A_{min}(\omega, q_*) = E(q_*) + \omega^2 G(q_*) + i\omega H(q_*) \in \mathbb{C}^{m \times m}$$

$$\begin{aligned} b_{min}(\omega, q_*) \\ = \beta_{min,1}(q_*) + \omega^2 \beta_{min,2}(q_*) + i\omega \beta_{min,3}(q_*) \end{aligned}$$

- Solve the (m x m) system

$$A_{min}(\omega, q_*)a = b_{min}(\omega, q_*)$$

- Effort:  $O(m^3)$  independent of full scale dimension = **real time online stage!**

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- **A practical example**
- Conclusions & Outlook

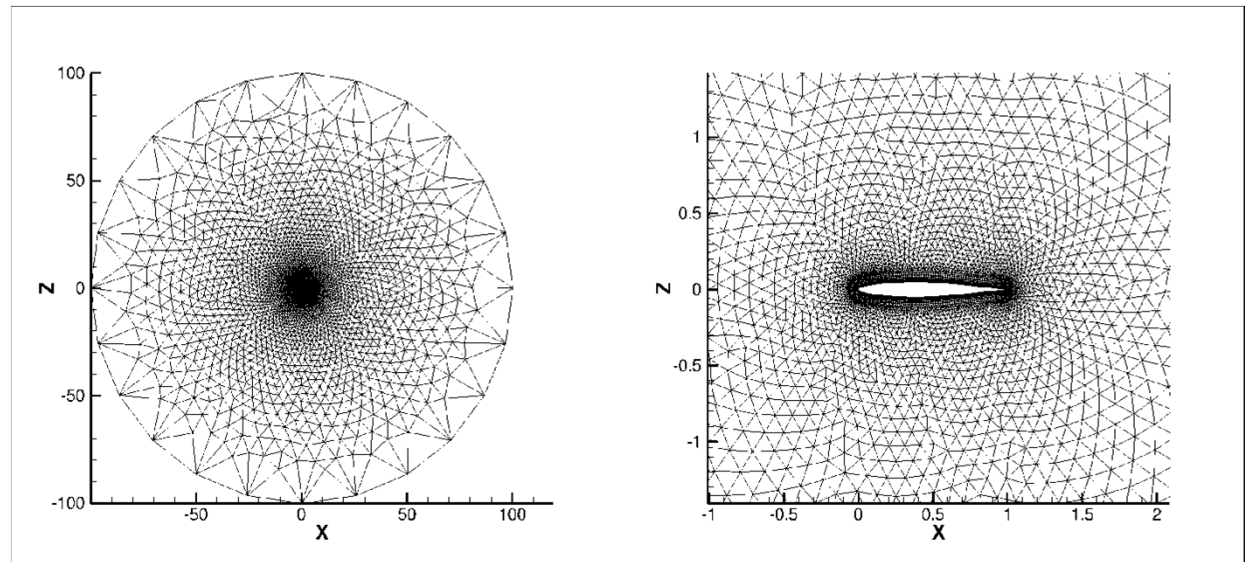
# A practical example

## Grassmann interpolation of ROBs for LFD approach to CFD

NACA64A010 airfoil:

Snapshots in transonic

Regime



2-parameter model:

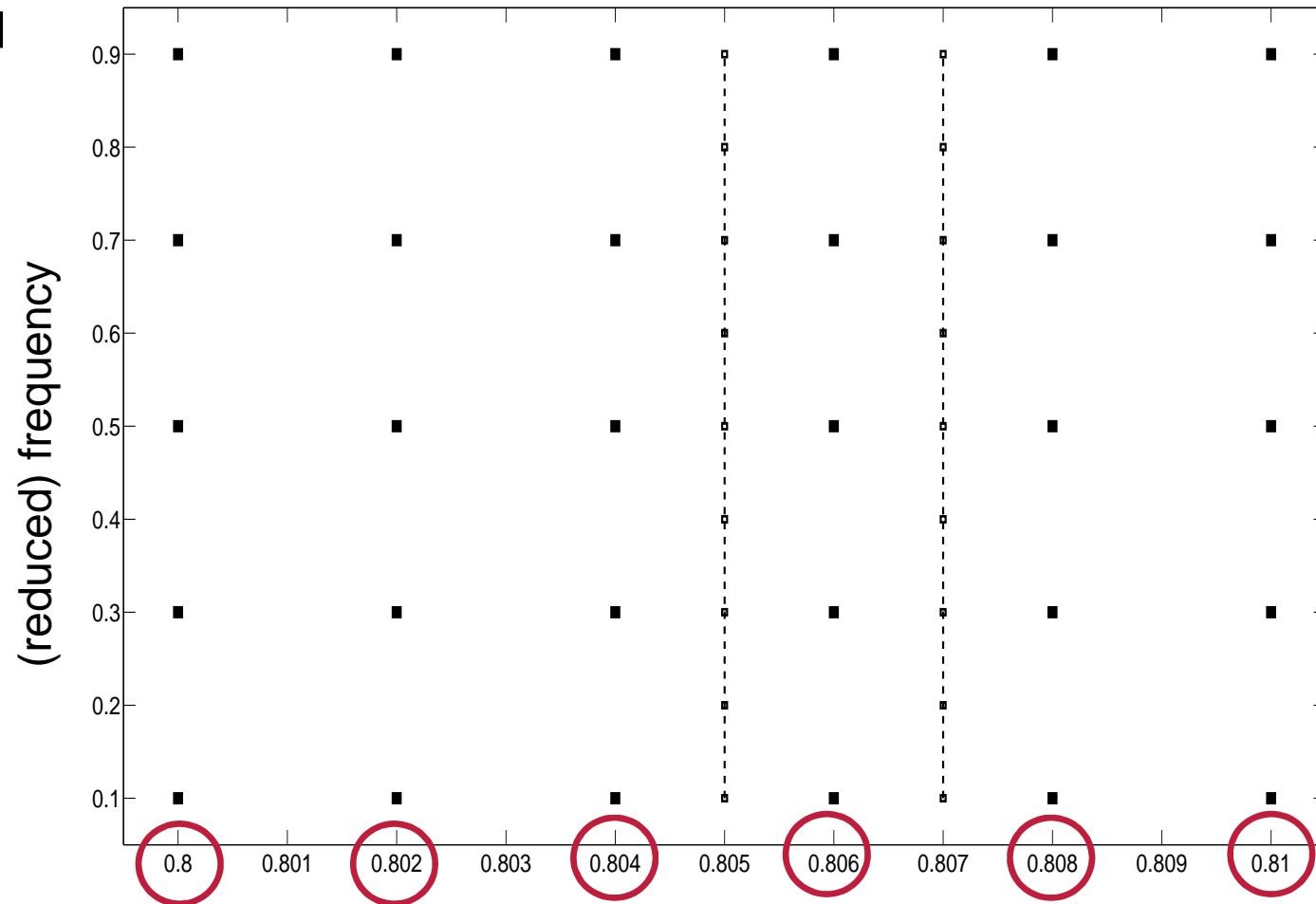
Computational grid, size: 10,727 points

$$Ma \in \{0.80, 0.802, 0.804, 0.806, 0.808, 0.81\}, \quad \kappa \in \{0.1, 0.3, 0.5, 0.7, 0.9\}$$

$$\bar{\alpha} \in 0^\circ, \quad Re \in 7.5mio \text{ fixed}$$

# A practical example

Snapshot and  
OP-bases  
sample plan

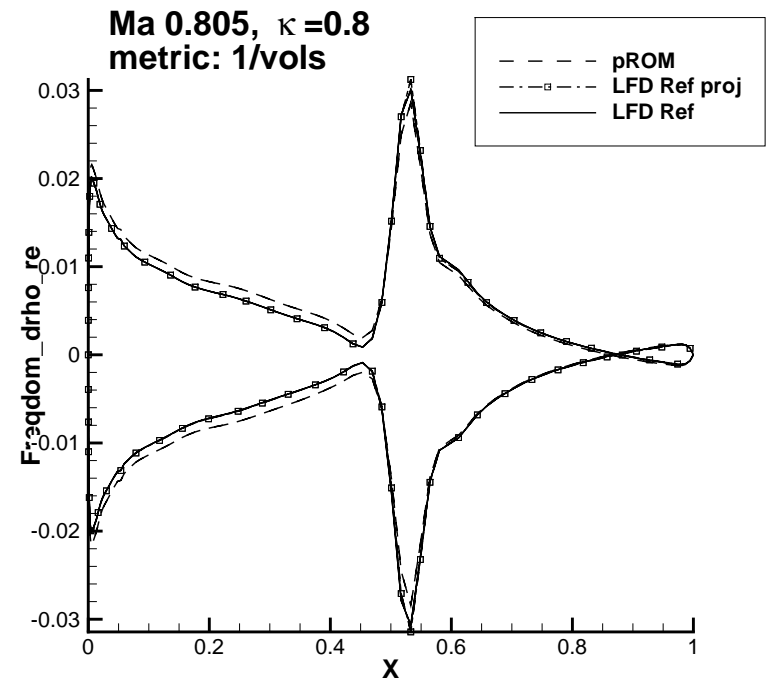
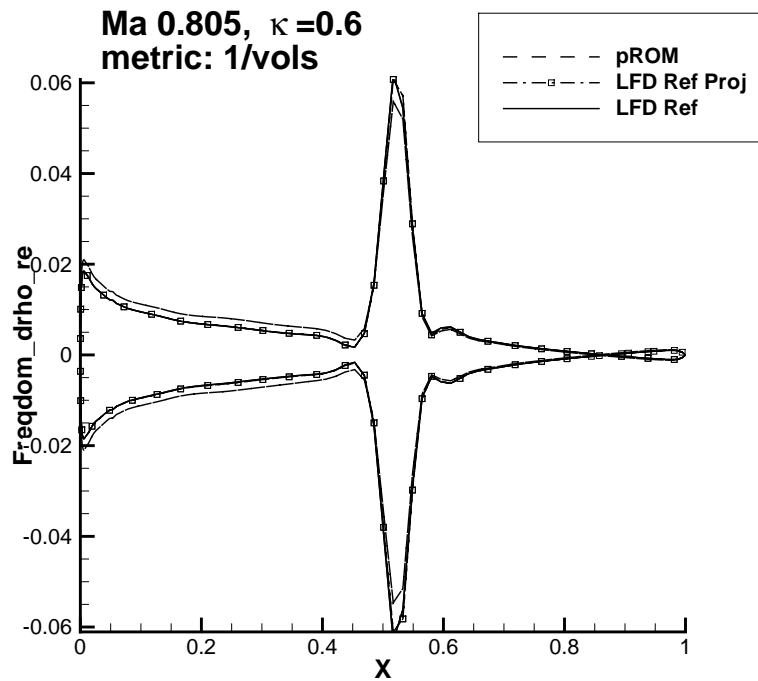
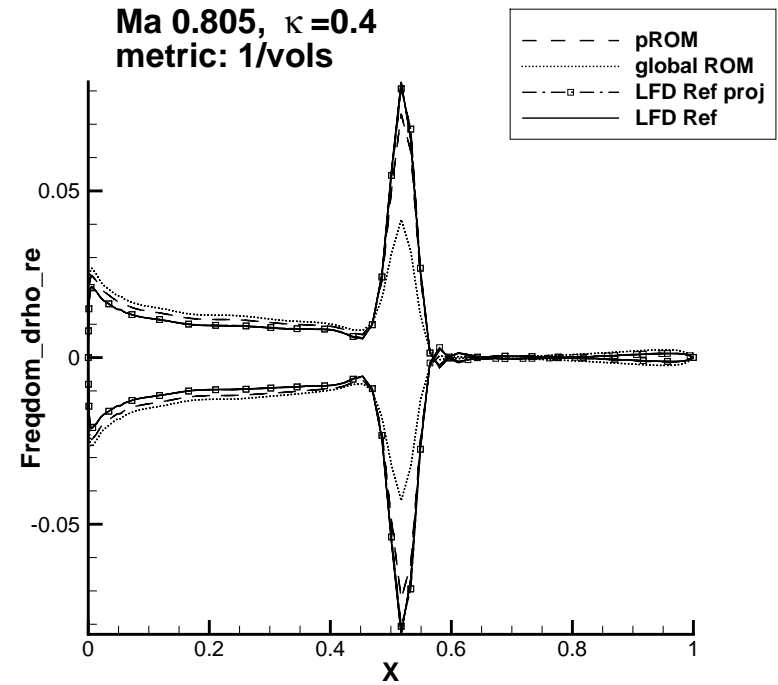
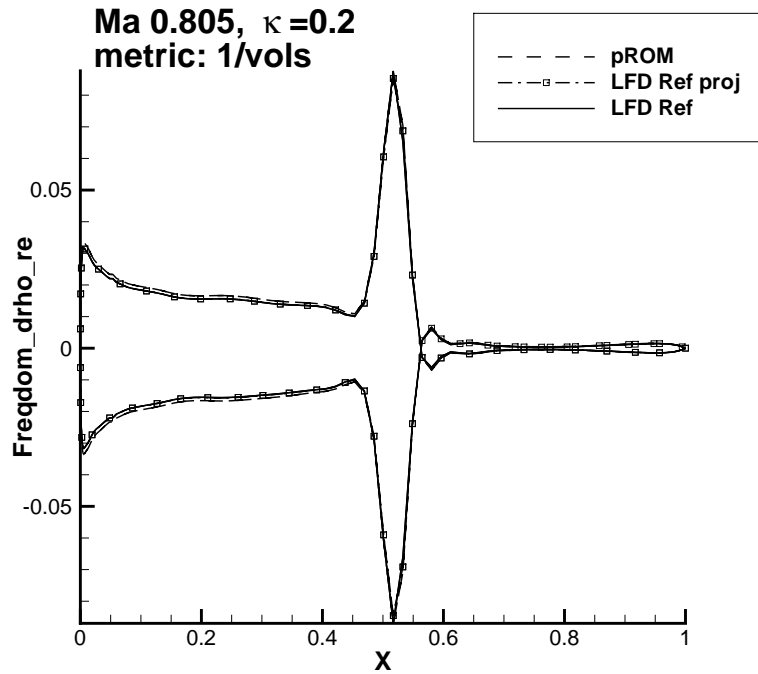


Sampled operating points defined by Mach number



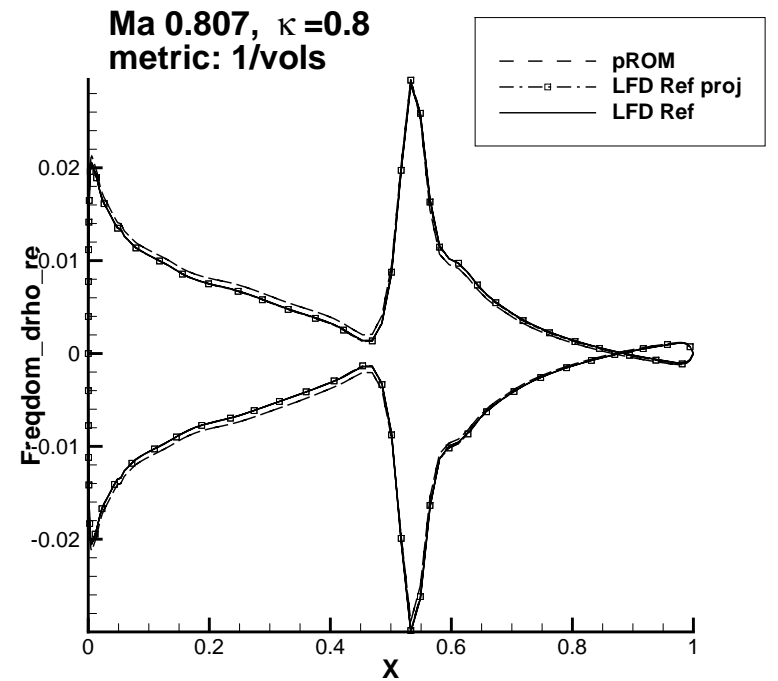
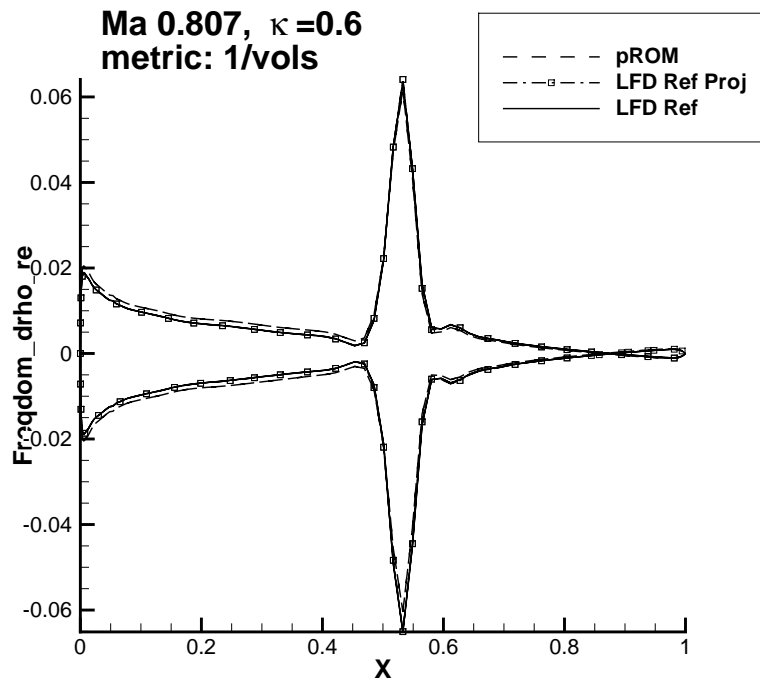
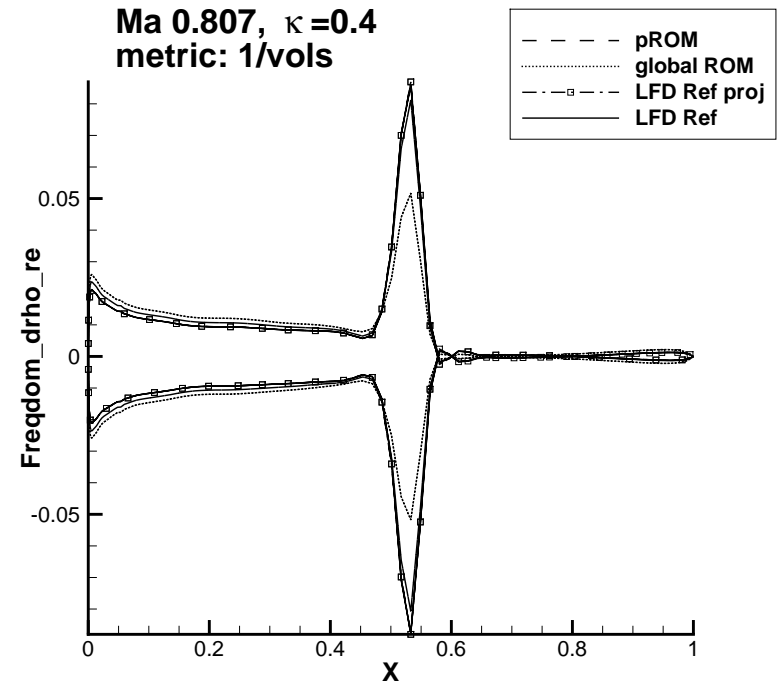
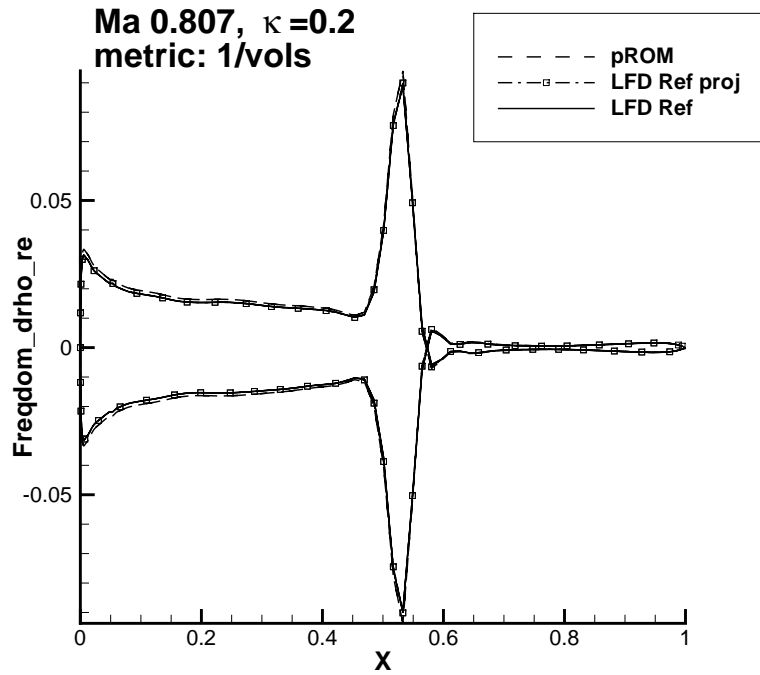
A practical example

$$\langle \cdot, \cdot \rangle = (\cdot)^T \bar{M}^{-1} (\cdot)$$



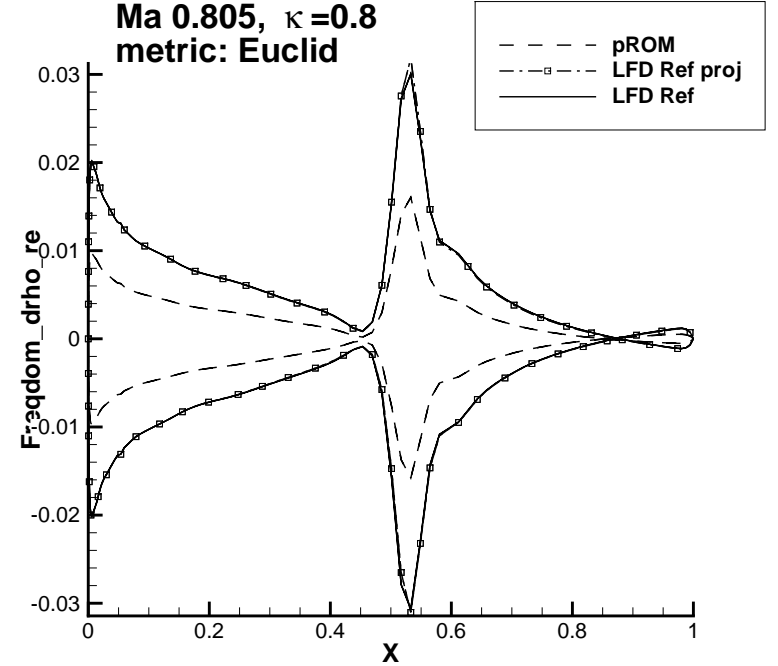
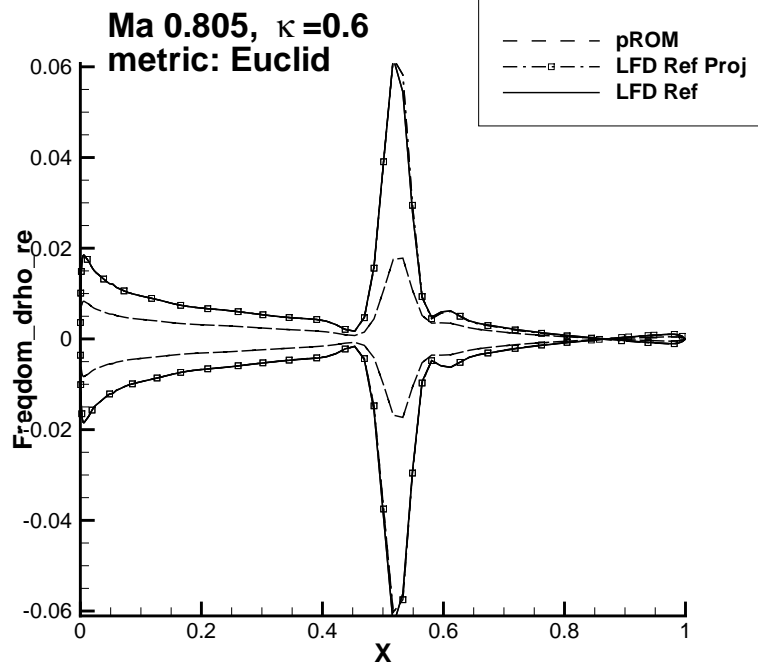
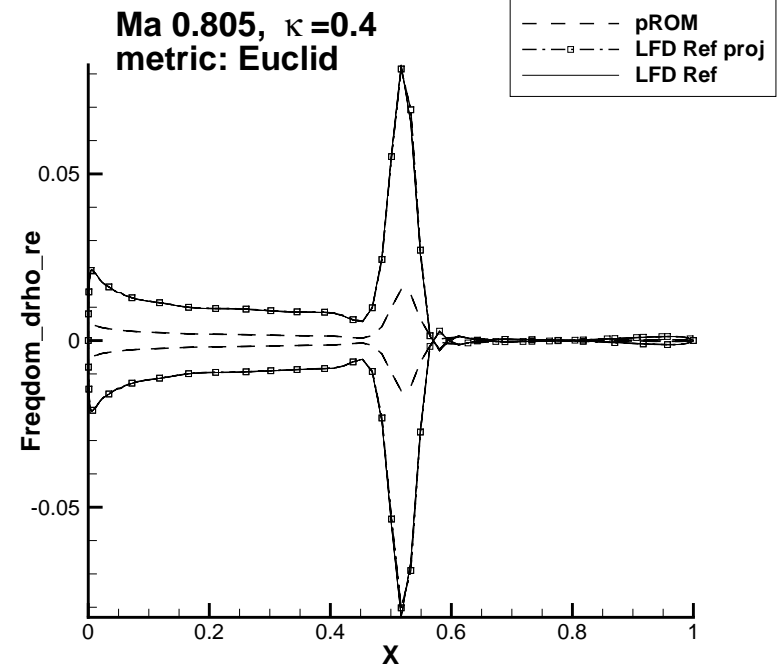
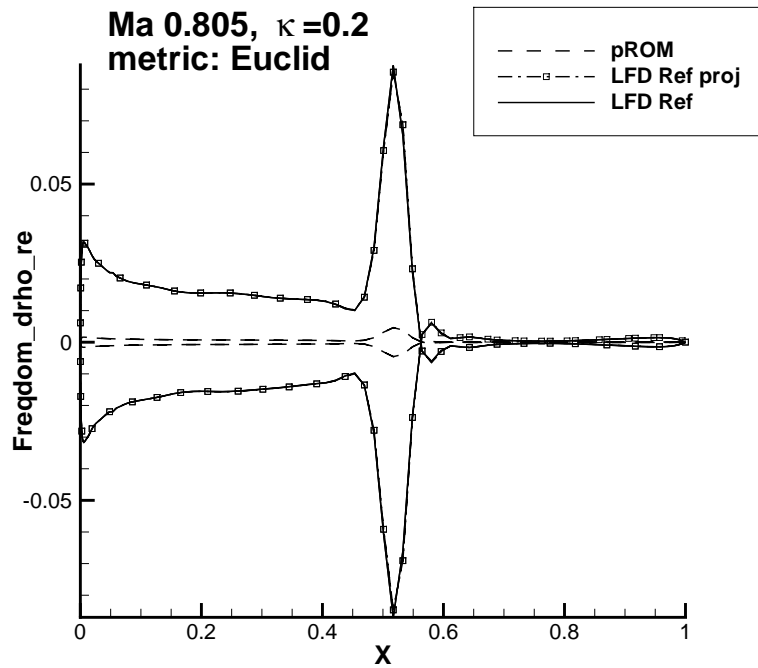
A practical example

$$\langle \cdot, \cdot \rangle = (\cdot)^T \bar{M}^{-1} (\cdot)$$



A practical example  
**Metrics matter!**

$$\langle \cdot, \cdot \rangle = (\cdot)^T (\cdot)$$

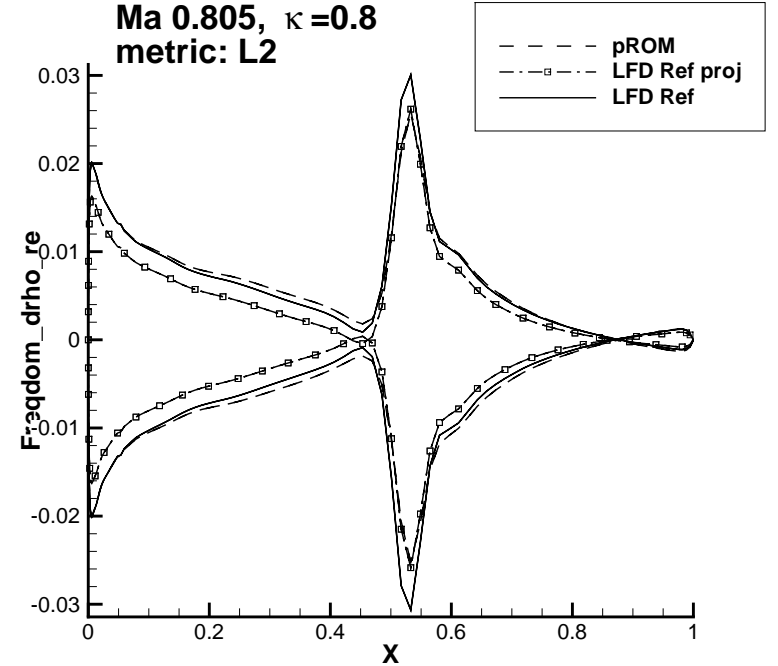
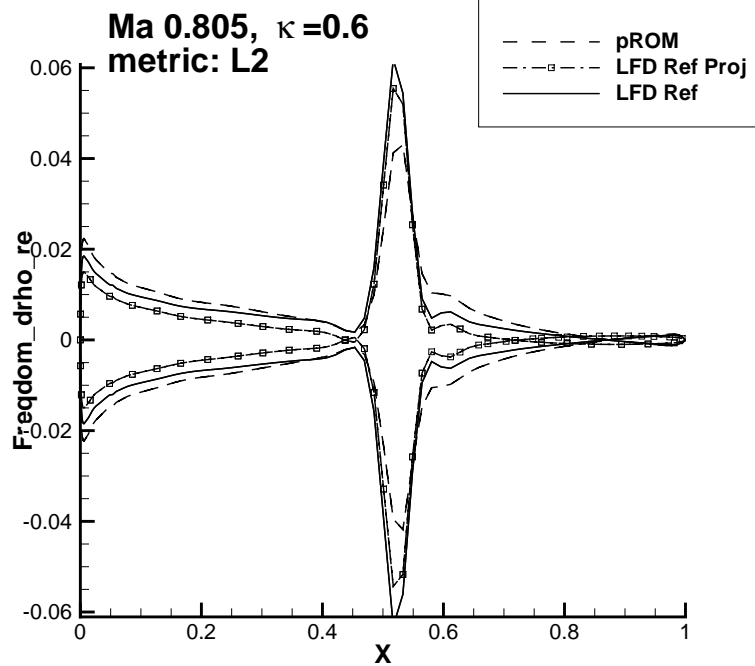
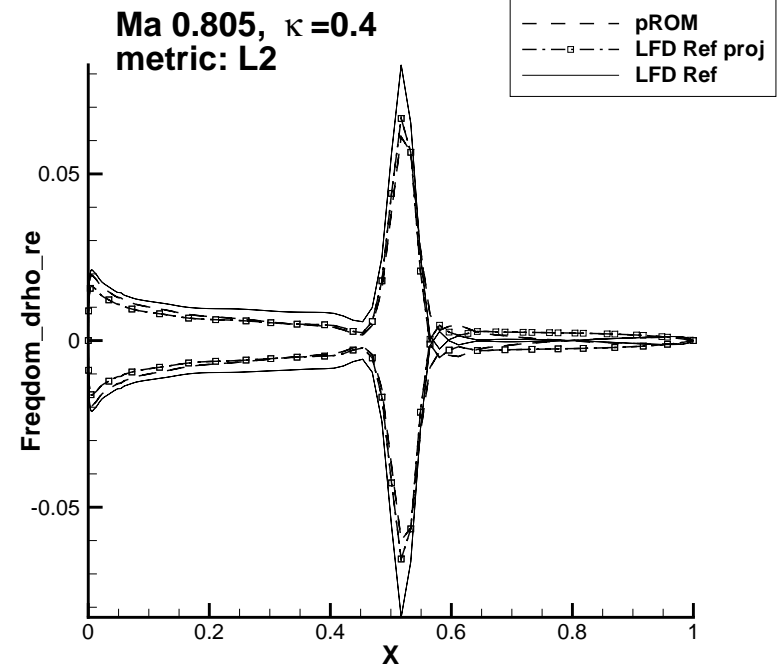
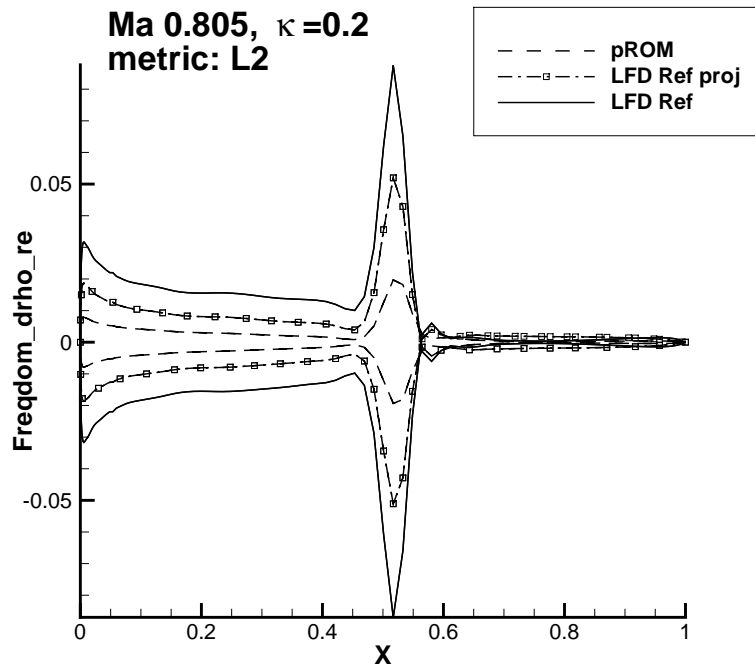


A practical example

**Metrics matter!**

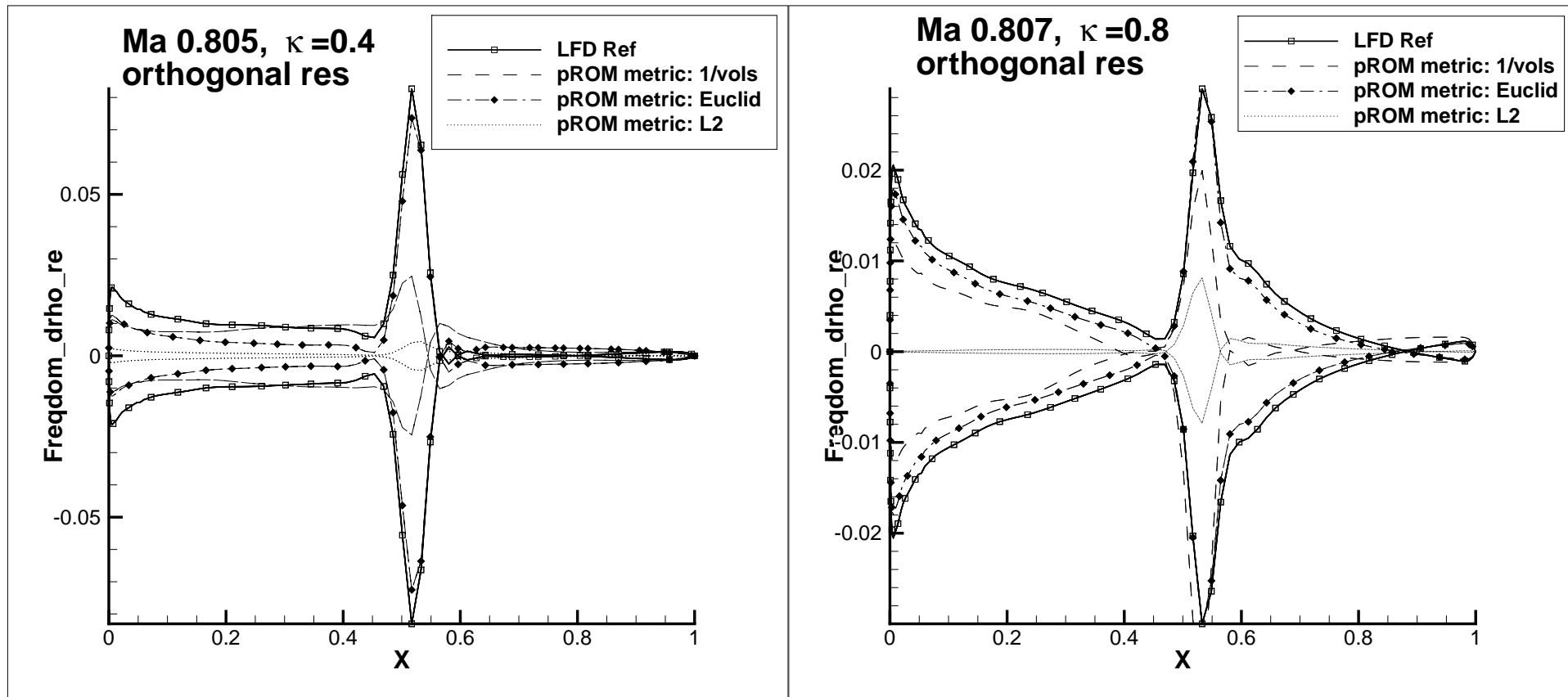
W.r.t. this metric, even the projection of the reference is quite off!

$$\langle \cdot, \cdot \rangle = (\cdot)^T \bar{M} (\cdot)$$



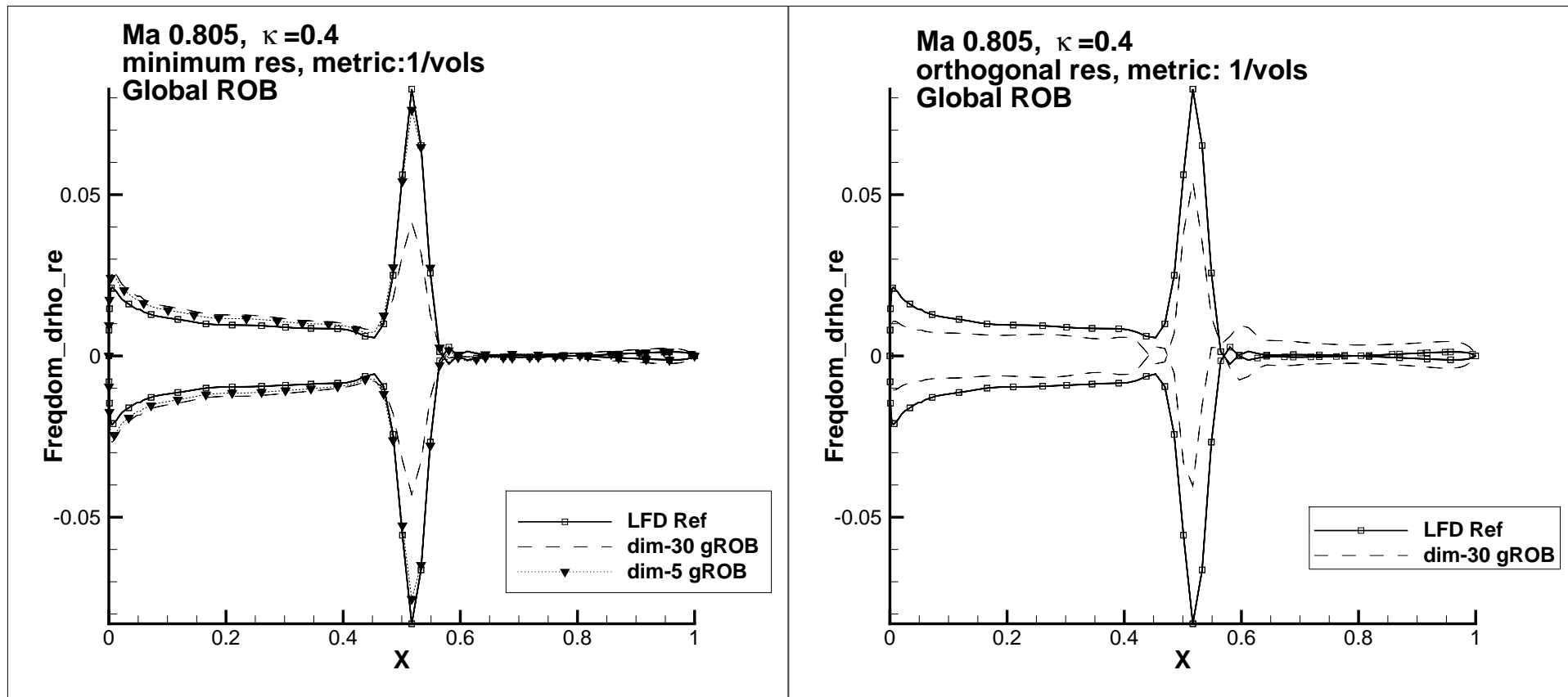
# A practical example

## The “orthogonal residual” approach is non-competitive



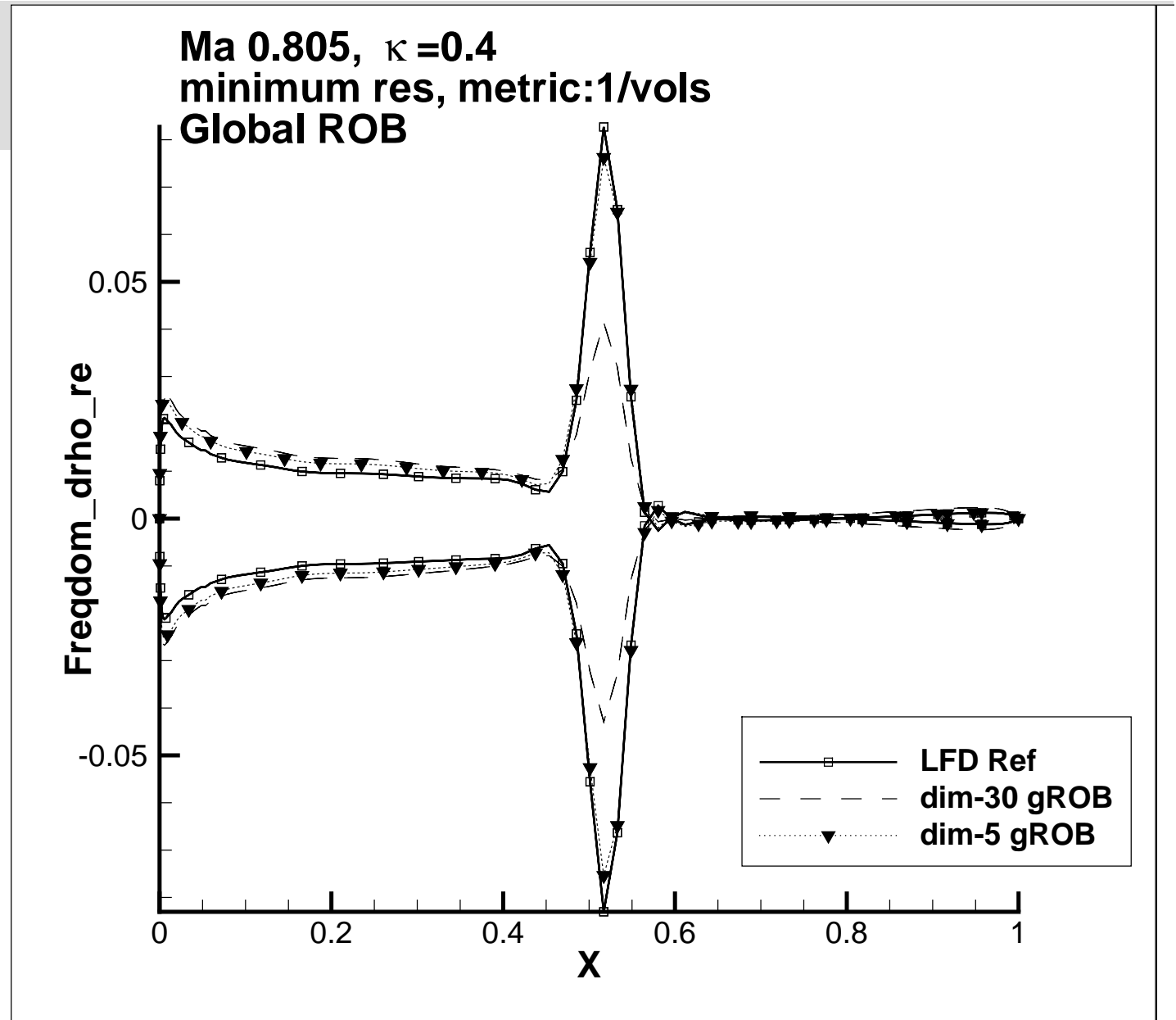
# A practical example

The “global 2D POD basis” approach is non-competitive



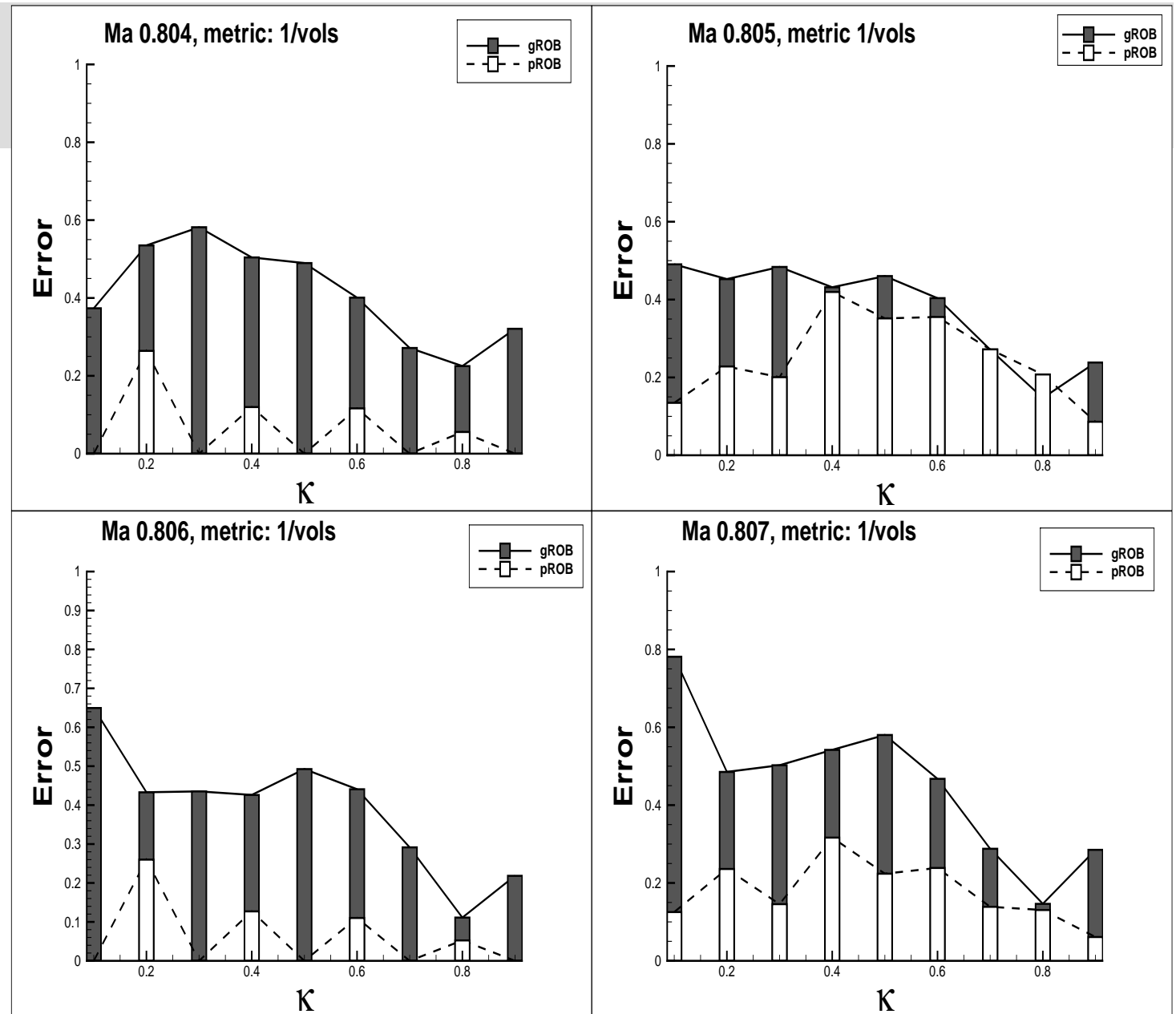
$$\langle \cdot, \cdot \rangle = (\cdot)^T \bar{M}^{-1} (\cdot)$$

The “reduced global 2D POD basis” approach **is competitive**, if only the 5 most dominant POD modes are kept, but...



$$\langle \cdot, \cdot \rangle = (\cdot)^T \bar{M}^{-1} (\cdot)$$

...any “global basis” approach lacks the interpolation property!





## Computational effort

- **Full order dimension:**  $5 \cdot 2 \cdot \#(\text{grid points}) = 107,270$
- **Reduced order dimension:**  $5(\text{complex}) = 10$  (real) at each OP

Timing results				
<b>Offline</b>				
	Mean flow	Full-order LFD	Complex POD	total
CPU time	~300s	5*35s	~0.26s	~475s (7min)
<b>Semi-offline</b>				
	Grassmann interp.	Reading system	Order reduction	
CPU time	~0.66s	~10.0s	~0.15s	~11s
<b>Online</b>				
	Set up ROM	Solve ROM	Build flow state	
CPU time	Below measure acc.	Below measure	0.01s	~0.01s

# Computational effort

- **Full order dimension:**  $5 \cdot 2 \cdot \#(\text{grid points}) = 107,270$
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<b>Online</b>				
	Set up ROM	Solve ROM	Build flow state	
CPU time	Below measure acc.	Below measure	0.01s	~0.01s

**Online speed up: factor ~3500**

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## Conclusions & Outlook

- Parametric ROM for LFD solver introduced
- Parameters of major interest (Mach, frequency) allow for a natural division into operation points and examination parameters
- **ROM** splits into **three** stages
  - **Offline**  
(provide snapshot data, compute projection bases)
  - **Semi-Offline**  
(precompute frequency-independent system parts, separable parameter dependency renders an interpolation of reduced systems as in [4,5] unnecessary)
  - **Online**  
(solve reduced system, real-time performance)

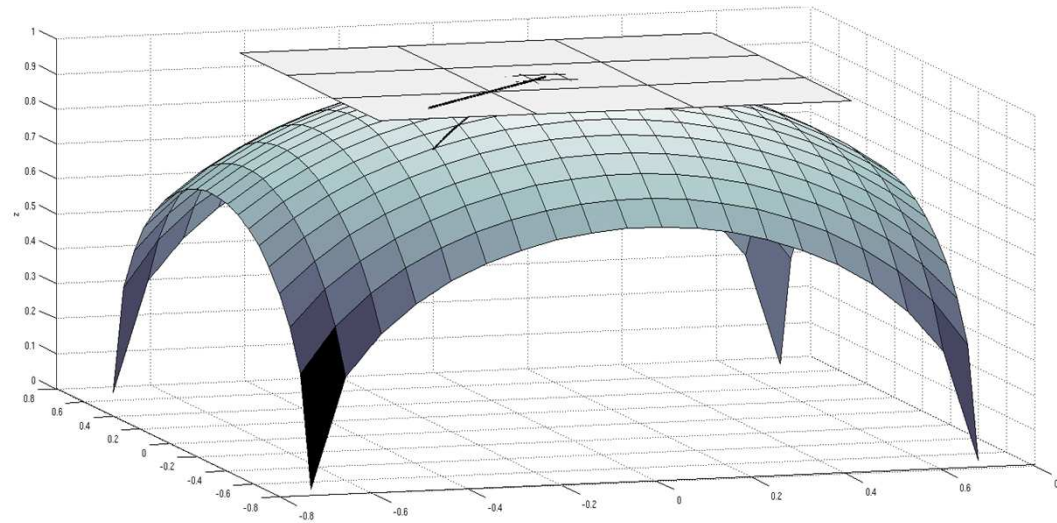
[4] Degroote J. et al., 2010

[5] Panzer, H. et al., 2010

## Conclusions & Outlook

- **Metric** proves to be essential in order to obtain good results  
(requires minor technical modifications, not shown here)
- **Minimum residual approach** outperforms **orthogonal residual approach**
- **Reduced global basis approach** gives satisfactory results, but underperforms when compared to **Grassmann interpolation**,  
(Necessarily lacks interpolation property)
- **Next step: geometrically optimized reduced order basis**

Thank you for your attention!



# An admissible interpolation scheme: radial basis functions

## Radial basis functions (RBF) in a nutshell

- Given:
  - Sample points  $p^1, \dots, p^k \in R^d$
  - Sample values  $y_1 = y(p^1), \dots, y_k = y(p^k) \in R$

- RBF interpolator:  $y^*(p) = (y_1, \dots, y_k) \Psi^{-1} \psi(p)$

$$\Psi = \left( r(\|p^i - p^j\|) \right)_{i,j \leq k} \in R^{k \times k}$$

$$\psi = \begin{pmatrix} r(\|p^1 - p\|) \\ \vdots \\ r(\|p^k - p\|) \end{pmatrix} \in R^k$$

# An admissible interpolation scheme: radial basis functions

## Application to Grassmann tangent vectors

- Given:
  - Sample points  $p^1, \dots, p^k \in R^d$
  - Sample values  $T^1 = T(p^1), \dots, T^k = T(p^k) \in R^{n \times m}$



# An admissible interpolation scheme: radial basis functions

## Application to Grassmann tangent vectors

- RBF interpolator:

$$\left( T_{i,j}^*(p) \right)_{i \leq n, j \leq m} = \left( (T_{i,j}^1, \dots, T_{i,j}^k) \Psi^{-1} \psi(p) \right)_{i \leq n, j \leq m}$$

$$= \left( (T_{:,j}^1, \dots, T_{:,j}^k) \Psi^{-1} \psi(p) \right)_{j \leq m}$$

$$= \left( \sum_{l=1}^k (\Psi^{-1} \psi(p))_l T_{:,1}^l, \dots, \sum_{l=1}^k (\Psi^{-1} \psi(p))_l T_{:,m}^l \right)$$

$$= \sum_{l=1}^k (e_l^T \Psi^{-1} \psi(p)) T^l \quad = \sum_{l=1}^k f_l(p) T^l$$

# An admissible interpolation scheme: radial basis functions

## ■ Conclusion

- RBF interpolation is admissible (so is e.g. linear interpolation)
- Entry-by-entry RBF interpolation tangent matrices  $\Leftrightarrow$  interpolating coefficients of linear expansion
- Associated computational effort:
  - $nm$  interpolation procedures, each for  $k$  sample points
  - vs.
  - $k$  interpolation procedures, each for  $k$  sample points