

On an inexact Newton-ADI solver for algebraic Riccati equations related to the LQR problem for linearized Navier-Stokes equations

Peter Benner Jens Saak Heiko K. Weichelt

Max Planck Institute for Dynamics of Complex Technical Systems Magdeburg,
Research group Computational Methods in Systems and Control Theory

Motivation (Test Scenarios)



Scenario 1: NSE on "von Kármán Vortex Street"

[BÄNSCH/BENNER/S./WEICHELDT 13]

PDE: NSE

Goal: $\vec{z} = \vec{v} - \vec{w} \rightarrow 0$

\rightsquigarrow Linearized Navier-Stokes equations:

$$\frac{\partial \vec{z}}{\partial t} - \frac{1}{\text{Re}} \Delta \vec{z} + (\vec{z} \cdot \nabla) \vec{w} + (\vec{w} \cdot \nabla) \vec{z} + \nabla p = 0$$

$$\text{div } \vec{z} = 0$$

defined on $(0, \infty) \times \Omega$

+ boundary and initial conditions

LQR

Minimize

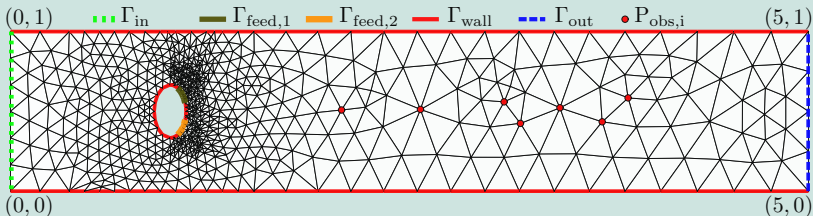
$$\mathcal{J}(\mathbf{y}, \mathbf{u}) = \frac{1}{2} \int_0^\infty \lambda \|\mathbf{y}\|^2 + \|\mathbf{u}\|^2 dt$$

s.t.

$$\begin{bmatrix} M_v & 0 \\ 0 & 0 \end{bmatrix} \frac{d}{dt} \begin{bmatrix} \mathbf{v} \\ \mathbf{p} \end{bmatrix} = \begin{bmatrix} A_v & G \\ G^T & 0 \end{bmatrix} \begin{bmatrix} \mathbf{v} \\ \mathbf{p} \end{bmatrix} + \begin{bmatrix} B_v \\ 0 \end{bmatrix} \mathbf{u}$$

$$\mathbf{y}(t) = C_v \mathbf{v}(t)$$

Domain Ω : von Kármán vortex street



Motivation (Test Scenarios)



Scenario 1: NSE "von Kármán Vortex Street"

[BÄNSCH/BENNER/S./WEICHELDT 13]

PDE: NSE

stationary NSE

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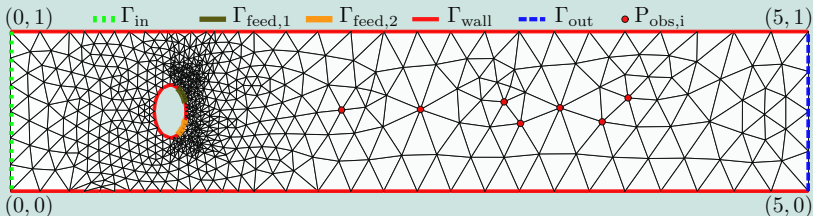
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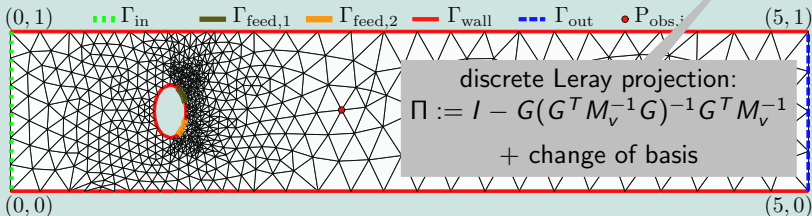
s.t.

$$\mathcal{M} \frac{d}{dt} \tilde{\mathbf{v}} = \mathcal{A} \tilde{\mathbf{v}} + \mathcal{B} \mathbf{u}$$

$$\mathbf{y}(t) = \mathcal{C} \tilde{\mathbf{v}}$$

[HEINKENSCHLOSS/SORENSEN/SUN '08]

Domain Ω : von Kármán vortex street



Motivation



Scenario 2: NSE Coupled with DCE in Reactor Model [BÄNSCH/BENNER/S./WEICHELDT 13-2]

PDE: NSE+DCE

Goal: $\vec{z} = \vec{v} - \vec{w} \rightarrow 0, c = c(\vec{v}) - c(\vec{w}) \rightarrow 0$

\rightsquigarrow Linearized coupled system:

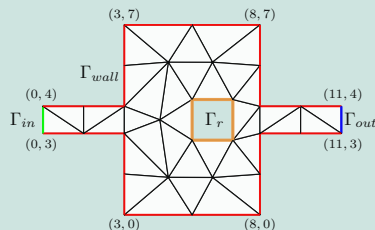
$$\frac{\partial \vec{z}}{\partial t} - \frac{1}{\text{Re}} \Delta \vec{z} + (\vec{z} \cdot \nabla) \vec{w} + (\vec{w} \cdot \nabla) \vec{z} + \nabla p = 0$$

$$\frac{\partial c}{\partial t} - \frac{1}{\text{ReSc}} \Delta c + (\vec{w} \cdot \nabla) c + (\vec{z} \cdot \nabla) c(\vec{w}) = 0$$

$$\text{div } \vec{z} = 0$$

defined on $(0, \infty) \times \Omega$ plus BC, IC

Domain Ω : Reactor Model



LQR

Minimize

$$\mathcal{J}(\mathbf{y}, \mathbf{u}) = \frac{1}{2} \int_0^{\infty} \lambda \|\mathbf{y}\|^2 + \|\mathbf{u}\|^2 dt$$

s.t.

$$\begin{bmatrix} M_v & 0 & 0 \\ 0 & M_c & 0 \\ 0 & 0 & 0 \end{bmatrix} \frac{d}{dt} \begin{bmatrix} \mathbf{v} \\ \mathbf{c} \\ \mathbf{p} \end{bmatrix} = \begin{bmatrix} A_v & 0 & G \\ -R & A_c & 0 \\ G^T & 0 & 0 \end{bmatrix} \begin{bmatrix} \mathbf{v} \\ \mathbf{c} \\ \mathbf{p} \end{bmatrix} + \begin{bmatrix} B_v \\ 0 \\ 0 \end{bmatrix} \mathbf{u}$$

$$\mathbf{y}(t) = C_c \mathbf{c}$$



Motivation

Scenario 2: NSE Coupled with DCE DCE Factor Model [BÄNSCH/BENNER/S./WEICHELDT 13-2]

PDE: NSE+DCE

stationary DCE in Ω : Reactor Model

Goal: $\vec{z} = \vec{v} - \vec{w} \rightarrow 0, c = c(\vec{v}) - c(\vec{w}) \rightarrow 0$

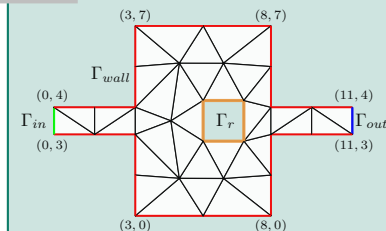
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LQR

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$$\begin{bmatrix} M_v & 0 & 0 \\ 0 & M_c & 0 \\ 0 & 0 & 0 \end{bmatrix} \frac{d}{dt} \begin{bmatrix} \mathbf{v} \\ \mathbf{c} \\ \mathbf{p} \end{bmatrix} = \begin{bmatrix} A_v & 0 & G \\ -R & A_c & 0 \\ G^T & 0 & 0 \end{bmatrix} \begin{bmatrix} \mathbf{v} \\ \mathbf{c} \\ \mathbf{p} \end{bmatrix} + \begin{bmatrix} B_v \\ 0 \\ 0 \end{bmatrix} \mathbf{u}$$

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Motivation



Scenario 2: NSE Coupled with DCE in Reactor Model [BÄNSCH/BENNER/S./WEICHELDT 13-2]

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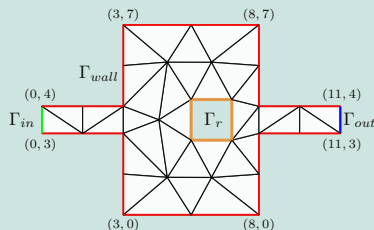
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Domain Ω : Reactor Model



LQR

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$$\mathcal{J}(\mathbf{y}, \mathbf{u}) = \frac{1}{2} \int_0^{\infty} \lambda \|\mathbf{y}\|^2 + \|\mathbf{u}\|^2 dt$$

s.t.

$$\mathcal{M} \frac{d}{dt} \begin{bmatrix} \tilde{\mathbf{v}} \\ \mathbf{c} \end{bmatrix} = \mathcal{A} \begin{bmatrix} \tilde{\mathbf{v}} \\ \mathbf{c} \end{bmatrix} + \begin{bmatrix} \mathcal{B} \\ \mathbf{0} \end{bmatrix} \mathbf{u}$$

$$\mathbf{y}(t) = C_c \mathbf{c}$$

[HEINKENSCHLOSS/SORENSEN/SUN '08]

Outline



- 1 Motivation
- 2 Discretized Control Systems
- 3 Nested Iteration
- 4 (Inexact) Newtons Method for AREs
- 5 Summary

Discretized Control Systems

Finite Element Discretization



- Standard FE discretization linearized (coupled) flow problems yields

$$M \frac{d}{dt} \mathbf{x}(t) = A \mathbf{x}(t) + \tilde{G} \mathbf{p}(t) + B \mathbf{u}(t) \quad (1a)$$

$$0 = G^T \mathbf{v}(t), \quad (1b)$$

$$\mathbf{y}(t) = C \mathbf{x}(t). \quad (1c)$$

Scenario 1

$$\mathbf{x}(t) = \mathbf{v}(t)$$

$$M = M_v$$

$$A = A_v$$

$$\tilde{G} = G$$

Scenario 2

$$\mathbf{x}(t) = \begin{bmatrix} \mathbf{v}(t) \\ \mathbf{c}(t) \end{bmatrix}$$

$$M = \begin{bmatrix} M_v & 0 \\ 0 & M_c \end{bmatrix}$$

$$A = \begin{bmatrix} A_v & 0 \\ -R & A_c \end{bmatrix}$$

$$\tilde{G} = \begin{bmatrix} G \\ 0 \end{bmatrix}$$

Discretized Control Systems



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Properties

- Differential algebraic system (DAE) of D-index 2 (iff \tilde{G} has full rank).
- Matrix pencil:

$$\left(\left[\begin{array}{cc} A & \tilde{G} \\ \tilde{G}^T & 0 \end{array} \right], \left[\begin{array}{cc} M & 0 \\ 0 & 0 \end{array} \right] \right).$$

Scenario 1

$$\mathbf{x}(t) = \mathbf{v}(t)$$

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- Descriptor system with multiple inputs and outputs (MIMO).

Discretized Control Systems



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- Descriptor system with multiple inputs and outputs (MIMO).
- Implicit index reduction to apply standard LQR approach

[HEINKENSCHLOSS/SORENSEN/SUN '08].

Discretized Control Systems



LQR Approach for Projected System

[BÄNSCH/BENNER/S./WEICHELDT 13]

Minimize

$$\mathcal{J}(\mathbf{y}, \mathbf{u}) = \frac{1}{2} \int_0^{\infty} \lambda \|\mathbf{y}\|^2 + \|\mathbf{u}\|^2 dt$$

subject to

$$\begin{aligned} \mathcal{M} \frac{d}{dt} \tilde{\mathbf{x}}(t) &= \mathcal{A} \tilde{\mathbf{x}}(t) + \mathcal{B} \mathbf{u}(t), \\ \mathbf{y}(t) &= \mathcal{C} \tilde{\mathbf{x}}(t). \end{aligned} \tag{2}$$

Discretized Control Systems



LQR Approach for Projected System

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Riccati Based Feedback Approach

(e.g.: [LOCATELLI '01])

- Optimal control: $\mathbf{u}(t) = -\mathcal{K} \tilde{\mathbf{x}}(t)$.
- Feedback: $\mathcal{K} = \mathcal{B}^T X \mathcal{M}$,

where X is the solution of the generalized algebraic Riccati equation

$$\mathcal{R}(X) = \mathcal{C}^T \mathcal{C} + \mathcal{A}^T X \mathcal{M} + \mathcal{M}^T X \mathcal{A} - \mathcal{M}^T X \mathcal{B} \mathcal{B}^T X \mathcal{M} = 0.$$

Nested Iteration – Overview



Compute feedback matrix $\mathcal{K} = \mathcal{B}^T X \mathcal{M}$ with X solves:

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Kleinman-Newton method

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Step (m + 1): solve Lyapunov equation [KLEINMAN '68]

$$(\mathcal{A} - \mathcal{B} \mathcal{K}^{(m)})^T X^{(m+1)} \mathcal{M} + \mathcal{M}^T X^{(m+1)} (\mathcal{A} - \mathcal{B} \mathcal{K}^{(m)}) = -(\mathcal{W}^{(m)})^T \mathcal{W}^{(m)}$$

Kleinman-Newton method

low rank ADI method



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Step i: solve the projected linear system

[BENNER/KÜRSCHNER/S. '13]

$$(\mathcal{A} - \mathcal{B}\mathcal{K}^{(m)} + q_i \mathcal{M})^T \mathcal{V}_i = \mathcal{Y}_{i-1} \quad (3)$$

Kleinman-Newton method

low rank ADI method

Krylov solver



Nested Iteration – Overview

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Avoid explicit projection using [HEINKENSCHLOSS/SORENSEN/SUN '08]:

Kleinman-Newton method

low rank ADI method

Krylov solver



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Step i: solve the projected linear system [BENNER/KÜRSCHNER/S. '13]

$$(\mathcal{A} - \mathcal{B}\mathcal{K}^{(m)} + q_i \mathcal{M})^T \mathcal{V}_i = \mathcal{Y}_{i-1} \quad (3)$$

Avoid explicit projection using [HEINKENSCHLOSS/SORENSEN/SUN '08]:

Replace (3) and solve instead the saddle point system (SPS)

Krylov solver

$$\begin{bmatrix} A^T - (K^{(m)})^T B^T + q_i M^T & \tilde{G} \\ \tilde{G}^T & 0 \end{bmatrix} \begin{bmatrix} V_i \\ * \end{bmatrix} = \begin{bmatrix} Y \\ 0 \end{bmatrix}$$

for different ADI shifts $q_i \in \mathbb{C}^-$ for a couple of rhs Y .

Kleinman-Newton method

low rank ADI method



Nested Iteration – Overview

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Step i: solve the projected linear system [BENNER/KÜRSCHNER/S. '13]

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Avoid explicit projection using [HEINKENSCHLOSS/SORENSEN/SUN '08]:

Replace (3) and solve instead the saddle point system (SPS)
(using Sherman Morrison Woodbury formula)

$$\begin{bmatrix} \mathcal{A}^T + q_i \mathcal{M}^T & \tilde{\mathcal{G}} \\ \tilde{\mathcal{G}}^T & 0 \end{bmatrix} \begin{bmatrix} \mathcal{V}_i \\ * \end{bmatrix} = \begin{bmatrix} \tilde{\mathcal{Y}} \\ 0 \end{bmatrix}$$

for different ADI shifts $q_i \in \mathbb{C}^-$ for a couple of rhs $\tilde{\mathcal{Y}}$.

Kleinman-Newton method

low rank ADI method

Krylov solver

Nested Iteration



Numerical Issues

Nested iteration depends on various parameters:

- Reynolds and Schmidt number (physical)
- ADI shifts q_i and refinement level (physical, FEM)
- regularization parameter λ (design)
- accuracy for Newton, ADI, and SPS iteration (experiences, nested influence)

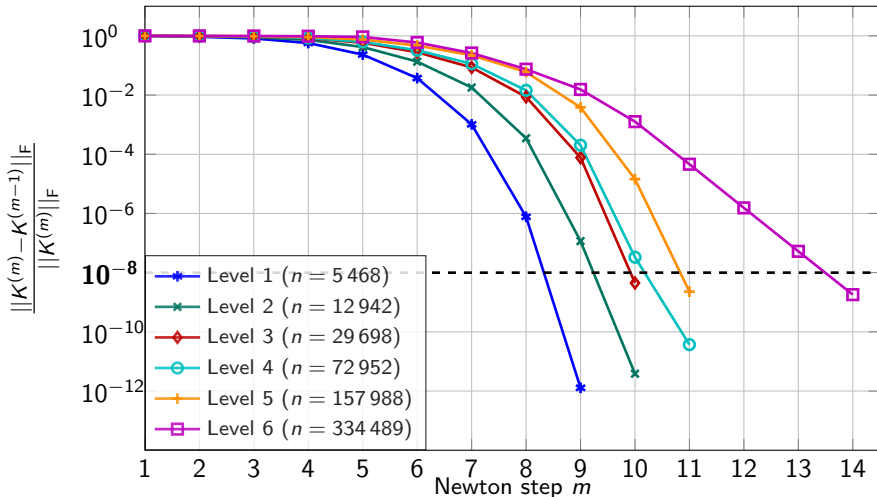
Selected Convergence Problems

- Newton-ADI vs. mesh refinement
- Newton-ADI vs. λ
- ADI vs. SPS solver

Nested Iteration

Newton-ADI vs. Mesh Refinement: Scenario 1

[BÄNSCH/BENNER/S./WEICHELT '13]



Relative change of feedback matrix K for different refinement levels

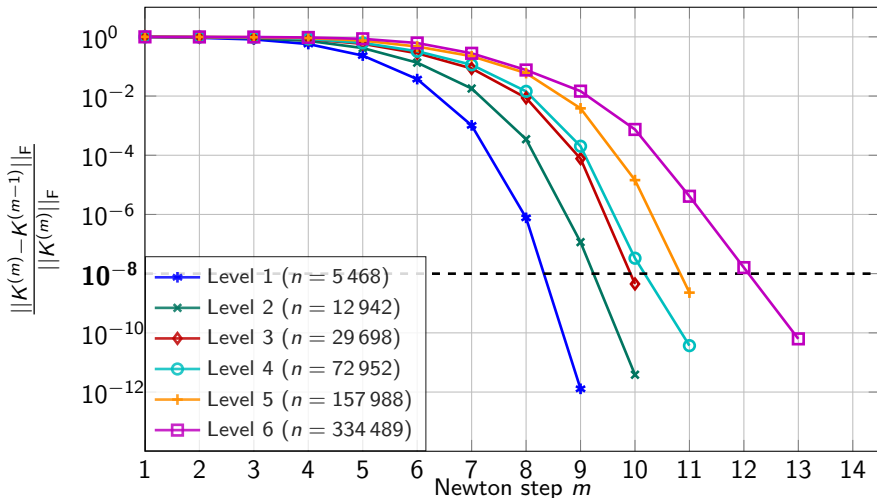
(Re = 500, $\lambda = 10^0$, $tol_{NM} = 10^{-8}$, $tol_{ADI} = 10^{-7}$).

Nested Iteration



Newton-ADI vs. Mesh Refinement: Scenario 1

[BÄNSCH/BENNER/S./WEICHELT '13]



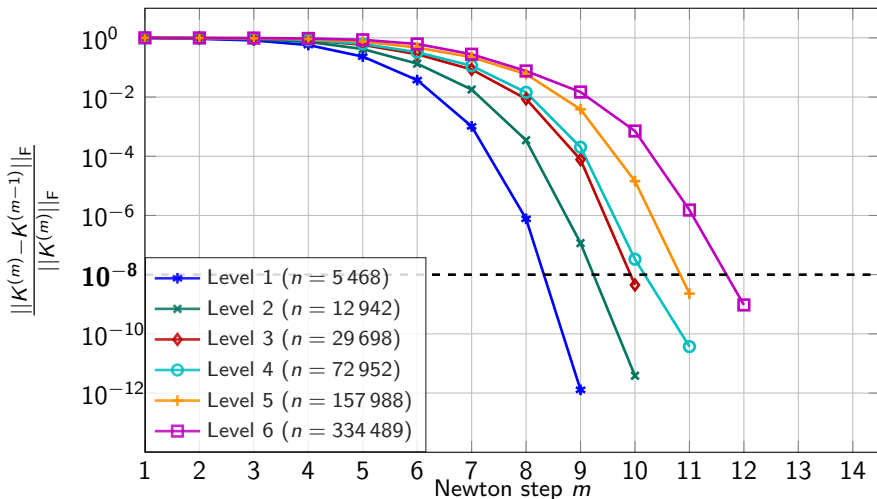
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Nested Iteration



Newton-ADI vs. Mesh Refinement: Scenario 1

[BÄNSCH/BENNER/S./WEICHELT '13]

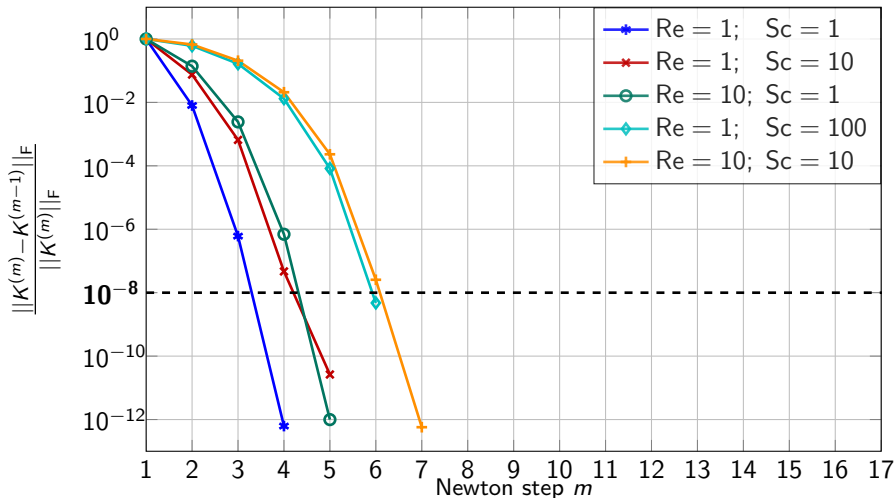


Relative change of feedback matrix K for different refinement levels
 ($\text{Re} = 500$, $\lambda = 10^0$, $\text{tol}_{\text{NM}} = 10^{-8}$, $\text{tol}_{\text{ADI}} = 10^{-9}$).

Nested Iteration

Newton-ADI vs. λ : Scenario 2

[BÄNSCH/BENNER/S./WEICHELDT '13-2]

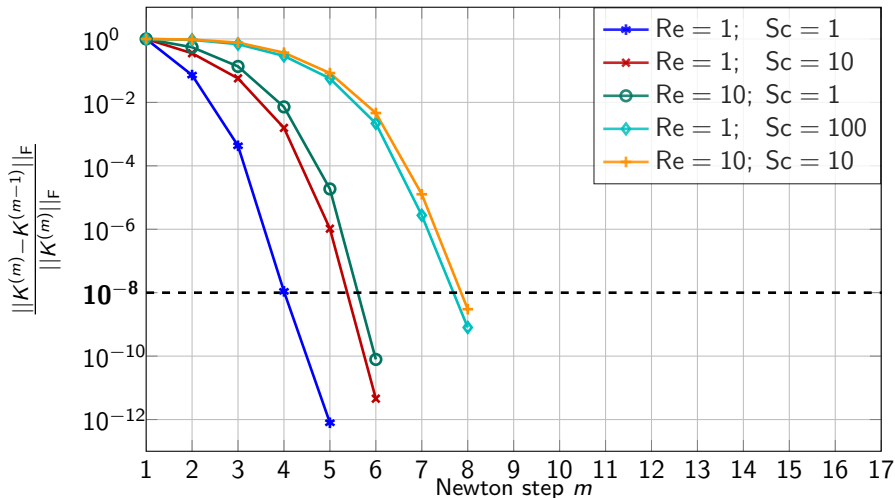


Relative change of feedback matrix K : $\lambda = 10^{-2}$
 ($n = 11\,555$, direct solver, $tol_{NM} = 10^{-8}$, $tol_{ADI} = 10^{-7}$).

Nested Iteration

Newton-ADI vs. λ : Scenario 2

[BÄNSCH/BENNER/S./WEICHELT '13-2]

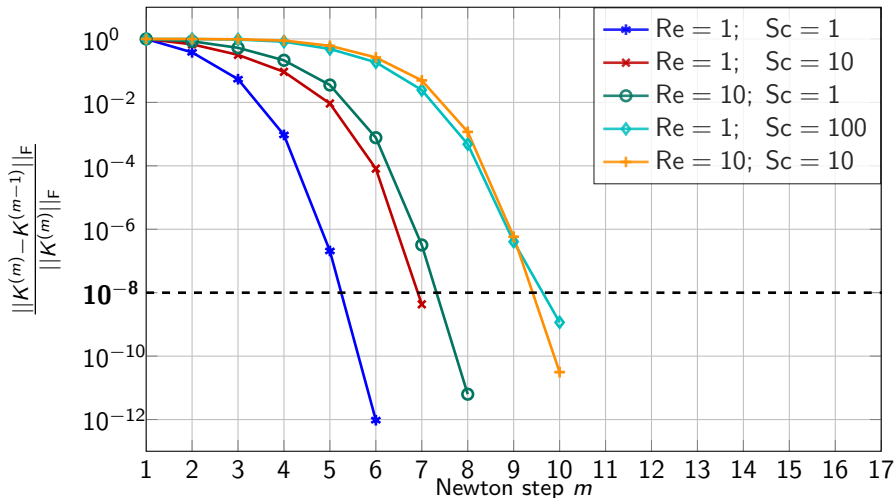


Relative change of feedback matrix K : $\lambda = 10^{-1}$
 ($n = 11\,555$, direct solver, $tol_{NM} = 10^{-8}$, $tol_{ADI} = 10^{-7}$).

Nested Iteration

Newton-ADI vs. λ : Scenario 2

[BÄNSCH/BENNER/S./WEICHELT '13-2]

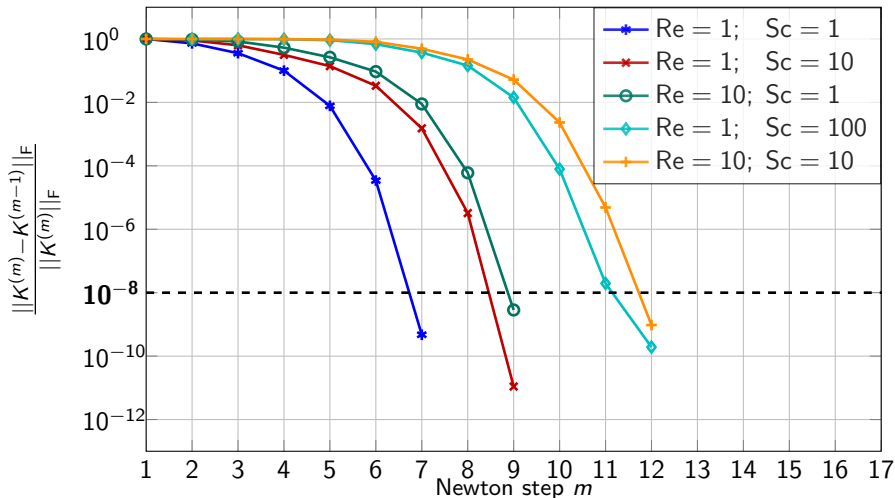


Relative change of feedback matrix K : $\lambda = 10^0$
 ($n = 11\,555$, direct solver, $tol_{NM} = 10^{-8}$, $tol_{ADI} = 10^{-7}$).

Nested Iteration

Newton-ADI vs. λ : Scenario 2

[BÄNSCH/BENNER/S./WEICHELT '13-2]

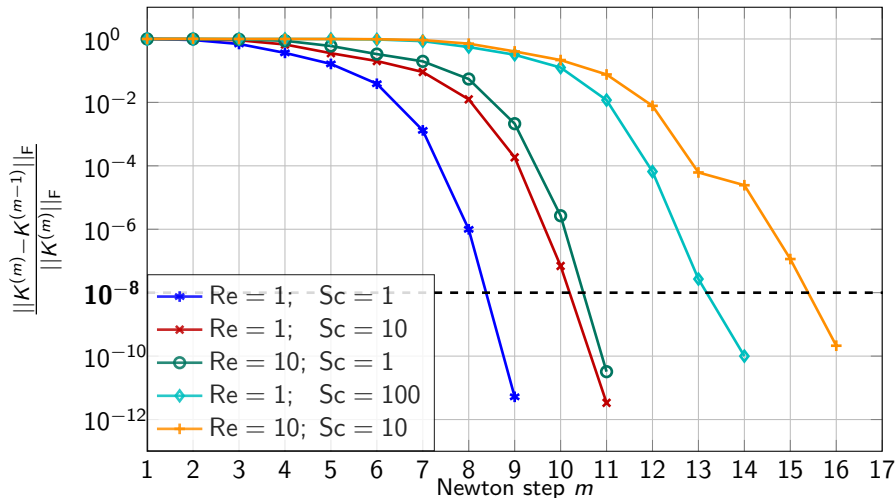


Relative change of feedback matrix K : $\lambda = 10^1$
 ($n = 11\,555$, direct solver, $tol_{NM} = 10^{-8}$, $tol_{ADI} = 10^{-7}$).

Nested Iteration

Newton-ADI vs. λ : Scenario 2

[BÄNSCH/BENNER/S./WEICHELT '13-2]



Relative change of feedback matrix K : $\lambda = 10^2$
 ($n = 11\,555$, direct solver, $tol_{NM} = 10^{-8}$, $tol_{ADI} = 10^{-7}$).

Nested Iteration



ADI vs. SPS solver: Stokes on Scenario 1

[BENNER/S./STOLL/WEICHELT '13]

tol_{SPS}	$\nu = 10^0$			$\nu = 10^{-1}$			$\nu = 10^{-2}$			$\nu = 10^{-3}$		
	n_N	n_A	time	n_N	n_A	time	n_N	n_A	time	n_N	n_A	time
10^{-5}	–	–	–	–	–	–	–	–	–	–	–	–
10^{-6}	–	–	–	12	343	536	17	645	1067	23	1266	2036
10^{-7}	7	144	279	11	273	504	17	525	1001	22	1004	1838
10^{-8}	7	139	304	11	247	520	17	457	998	22	686	1413
10^{-9}	7	139	342	11	247	580	17	434	1074	22	616	1437
10^{-10}	7	138	374	11	247	638	17	434	1167	22	612	1568
10^{-11}	7	138	405	11	247	693	17	434	1222	22	612	1707
10^{-12}	7	138	442	11	247	756	17	434	1312	22	606	1856
direct	7	138	/	11	247	/	17	434	/	22	606	/

Table: Number of Newton and ADI steps for varying accuracy of GMRES.

(Inexact) Newton Methods for AREs



Basic Concepts

[KLEINMAN '68, FEITZINGER/HYLLA/SACHS '09]

Consider

$$\mathcal{R}(X) := C^T C + A^T X M + M^T X A - M^T X B B^T X M = 0$$

Inexact Kleinman's Iteration for the ARE

$$\mathcal{R}'|_{X^{(m)}}(X^{(m+1)}) - \mathcal{R}'|_{X^{(m)}}(X^{(m)}) + \mathcal{R}(X^{(m)}) = R^{(m)}, \quad m = 0, 1, \dots$$

i.e., in every Newton step (**approximately**) solve a

Lyapunov Equation

$$(\mathcal{F}^{(m)})^T X^{(m+1)} M + M^T X^{(m+1)} \mathcal{F}^{(m)} = \\ -(\mathcal{W}^{(m)})^T \mathcal{W}^{(m)} + R^{(m)}.$$

(Inexact) Newtons Method for AREs



Convergence Result [KLEINMAN '68, LANCASTER/RODMAN '95, FEITZINGER/HYLLA/SACHS '09]

Theorem

Let Assumption 1 hold,

$$0 \leq R^{(m)} \leq C^T C \quad \text{and} \quad 0 \leq R^{(m)} \leq M^T N^{(m)} B B^T N^{(m)} M.$$

Then the iterates defined by

$$(\mathcal{F}^{(m)})^T X^{(m+1)} + X^{(m+1)} \mathcal{F}^{(m)} = -(\mathcal{W}^{(m)})^T \mathcal{W}^{(m)} + R^{(m)},$$

converge to the unique symmetric matrix $X^{(\infty)}$, such that

- $\mathcal{R}(X^{(\infty)}) = 0$
- and $A - B B^T X^{(\infty)} M$ is stable.

Furthermore the convergence is *quadratic* and *monotone* with

$$0 \leq X^{(\infty)} \leq \dots \leq X^{(m+1)} \leq X^{(m)} \leq \dots \leq X^{(1)}.$$

(Inexact) Newtons Method for AREs



Convergence Result (Remarks)

Weaker Condition

[HYLLA '10]

Replacing

$$R^{(m)} \leq c^T c$$

by

$$R^{(m)} \leq c^T c + (\mathcal{K}^{(m)})^T \mathcal{K}^{(m)}$$

keeps the iteration well defined.

(Inexact) Newtons Method for AREs



Convergence Result (Remarks)

Weaker Condition

[HYLLA '10]

Replacing

$$R^{(m)} \leq C^T C$$

by

$$R^{(m)} \leq C^T C + (\mathcal{K}^{(m)})^T \mathcal{K}^{(m)}$$

keeps the iteration well defined.

Large Scale Difficulty $R^{(m)} = \mathcal{Y}_{n_A} \mathcal{Y}_{n_A}^T$, but column spans are unrelated

In general none of the conditions

- $R^{(m)} \leq C^T C$,
- $R^{(m)} \leq C^T C + (\mathcal{K}^{(m)})^T \mathcal{K}^{(m)}$,
- $0 \leq R^{(m)} \leq \mathcal{M}^T N^{(m)} \mathcal{B} \mathcal{B}^T N^{(m)} \mathcal{M}$,

can hold in large scale applications.

(Inexact) Newtons Method for AREs



Accuracy control for the (G-)LRCF-ADI

Main Problem:

Can we enforce quadratic convergence without checking

$$0 \leq R^{(m)} \leq C^T C \quad \text{and} \quad 0 \leq R^{(m)} \leq M^T N^{(m)} B B^T N^{(m)} M?$$

(Inexact) Newtons Method for AREs



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$$0 \leq R^{(m)} \leq C^T C \quad \text{and} \quad 0 \leq R^{(m)} \leq M^T N^{(m)} B B^T N^{(m)} M?$$

Due to the quadratic nature of $\mathcal{R}(\cdot)$ we have

$$\mathcal{R}(Y) = \mathcal{R}(X) + \mathcal{R}'|_X(Y - X) + \frac{1}{2} \mathcal{R}''|_X(Y - X, Y - X).$$

(Inexact) Newtons Method for AREs



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Recall the Inexact Kleinman step:

$$R^{(m)} = \mathcal{R}'|_{X^{(m)}}(X^{(m+1)}) - \mathcal{R}'|_{X^{(m)}}(X^{(m)}) + \mathcal{R}(X^{(m)})$$

(Inexact) Newtons Method for AREs



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Recall the Inexact Kleinman step:

$$R^{(m)} = \mathcal{R}(X^{(m)}) + \mathcal{R}'|_{X^{(m)}}(X^{(m+1)} - X^{(m)})$$

(Inexact) Newtons Method for AREs



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$$R^{(m)} = \mathcal{R}(X^{(m)}) + \mathcal{R}'|_{X^{(m)}}(X^{(m+1)} - X^{(m)})$$

and thus

$$\mathcal{R}(X^{(m+1)}) = R^{(m)} + \frac{1}{2} \mathcal{R}''|_{X^{(m)}}(X^{(m+1)} - X^{(m)}, X^{(m+1)} - X^{(m)}).$$

(Inexact) Newtons Method for AREs



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Due to the quadratic nature of $\mathcal{R}(\cdot)$ we have

$$\mathcal{R}(Y) = \mathcal{R}(X) + \mathcal{R}'|_X(Y - X) + \frac{1}{2} \mathcal{R}''|_X(Y - X, Y - X).$$

Recall the Inexact Kleinman step:

$$R^{(m)} = \mathcal{R}(X^{(m)}) + \mathcal{R}'|_{X^{(m)}}(X^{(m+1)} - X^{(m)})$$

and thus

$$\mathcal{R}(X^{(m+1)}) = R^{(m)} - M^T N^{(m)} B B^T N^{(m)} M.$$



(Inexact) Newtons Method for AREs

Accuracy control for the (G-)LRFCF-ADI

Riccati residual

inner Lyapunov residual

New Question

How can we exploit $\mathcal{R}(X^{(m+1)}) = \mathcal{R}^{(m)} - \mathcal{M}N^{(m)}BB^T N^{(m)}\mathcal{M}$ to control the ADI accuracy?

$$\begin{aligned}
 \mathcal{M}^T N^{(m)} B B^T N^{(m)} \mathcal{M} &= \mathcal{M}^T (X^{(m+1)} - X^{(m)}) B B^T (X^{(m+1)} - X^{(m)}) \mathcal{M} \\
 &= (\mathcal{K}^{(m+1)})^T \mathcal{K}^{(m+1)} + (\mathcal{K}^{(m)})^T \mathcal{K}^{(m)} \\
 &\quad - (\mathcal{K}^{(m+1)})^T \mathcal{K}^{(m)} - (\mathcal{K}^{(m)})^T \mathcal{K}^{(m+1)} \\
 &= (\Delta \mathcal{K}^{(m+1)})^T \Delta \mathcal{K}^{(m+1)}
 \end{aligned}$$



(Inexact) Newtons Method for AREs

Accuracy control for the (G-)LRFCF-ADI

Riccati residual

inner Lyapunov residual

New Question

How can we exploit $\mathcal{R}(X^{(m+1)}) = \mathcal{R}^{(m)} - \mathcal{M}N^{(m)}BB^T N^{(m)}\mathcal{M}$ to control the ADI accuracy?

$$\begin{aligned} \mathcal{M}^T N^{(m)} B B^T N^{(m)} \mathcal{M} &= \mathcal{M}^T (X^{(m+1)} - X^{(m)}) B B^T (X^{(m+1)} - X^{(m)}) \mathcal{M} \\ &= (\mathcal{K}^{(m+1)})^T \mathcal{K}^{(m+1)} + (\mathcal{K}^{(m)})^T \mathcal{K}^{(m)} \\ &\quad - (\mathcal{K}^{(m+1)})^T \mathcal{K}^{(m)} - (\mathcal{K}^{(m)})^T \mathcal{K}^{(m+1)} \\ &= (\Delta \mathcal{K}^{(m+1)})^T \Delta \mathcal{K}^{(m+1)} \end{aligned}$$

Key Idea:

$$\|\mathcal{R}(X^{(m+1)})\| = \|\mathcal{R}^{(m)} - (\Delta \mathcal{K}^{(m+1)})^T \Delta \mathcal{K}^{(m+1)}\| \leq \alpha \|\mathcal{R}(X^{(m)})\|^2$$

(Inexact) Newtons Method for AREs



Accuracy control for the (G-)LRCF-ADI

Overestimation approach

(good steps are bad)

$$\|\mathcal{R}(X^{(m+1)})\| \leq \|R^{(m)}\| + \|(\Delta\mathcal{K}^{(m+1)})^T \Delta\mathcal{K}^{(m+1)}\| \leq \alpha \|\mathcal{R}(X^{(m)})\|^2$$

(Inexact) Newtons Method for AREs

Accuracy control for the (G-)LRCF-ADI



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(good steps are bad)

$$\|\mathcal{R}(X^{(m+1)})\| \leq \|R^{(m)}\| + \|(\Delta\mathcal{K}^{(m+1)})^T \Delta\mathcal{K}^{(m+1)}\| \leq \alpha \|\mathcal{R}(X^{(m)})\|^2$$

Low-rank residual approach

(several version with disadvantages)

$$\begin{aligned} \|R^{(m)} - (\Delta\mathcal{K}^{(m+1)})^T \Delta\mathcal{K}^{(m+1)}\| &= \|\mathcal{Y}^{(m)}(\mathcal{Y}^{(m)})^T - (\Delta\mathcal{K}^{(m+1)})^T \Delta\mathcal{K}^{(m+1)}\| \\ &= \|\mathcal{U}^{(m)}(\mathcal{U}^{(m)})^T\| \\ \mathcal{U}^{(m)} &= [\mathcal{Y}^{(m)}, \iota(\Delta\mathcal{K}^{(m+1)})^T] \end{aligned}$$



(Inexact) Newtons Method for AREs

Accuracy control for the (G-)LRFCF-ADI

Overestimation approach

(good steps are bad)

$$\|\mathcal{R}(X^{(m+1)})\| \leq \|R^{(m)}\| + \|(\Delta\mathcal{K}^{(m+1)})^T \Delta\mathcal{K}^{(m+1)}\| \leq \alpha \|\mathcal{R}(X^{(m)})\|^2$$

Low-rank residual approach

(several version with disadvantages)

$$\begin{aligned} \|R^{(m)} - (\Delta\mathcal{K}^{(m+1)})^T \Delta\mathcal{K}^{(m+1)}\| &= \|\mathcal{Y}^{(m)}(\mathcal{Y}^{(m)})^T - (\Delta\mathcal{K}^{(m+1)})^T \Delta\mathcal{K}^{(m+1)}\| \\ &= \|\mathcal{U}^{(m)}(\mathcal{U}^{(m)})^T\| \\ \mathcal{U}^{(m)} &= [\mathcal{Y}^{(m)}, \iota(\Delta\mathcal{K}^{(m+1)})^T] \end{aligned}$$

- $\|\cdot\| = \|\cdot\|_2 \rightsquigarrow$ eigensolver convergence?
- \mathcal{U} is complex \rightsquigarrow *wrong* outer product
- $\|\cdot\| = \|\cdot\|_F \rightsquigarrow$ inner product version reformulation may suffer from numerical cancelation?

(Inexact) Newtons Method for AREs



Accuracy Control of the SPS Solver

Exact Solution of the SPS

[BENNER/KÜRSCHNER/S. '13]

- $\mathcal{Z}_i^{(m)} = [\mathcal{V}_1, \mathcal{V}_2, \dots, \mathcal{V}_i]$.
- $\text{rank}(R^{(m)}) = \text{rank}(\mathcal{Y}_i^{(m)}) = p + q \quad (B \in \mathbb{R}^{n \times p}, C \in \mathbb{R}^{q \times n})$,

(Inexact) Newtons Method for AREs

Accuracy Control of the SPS Solver



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[BENNER/KÜRSCHNER/S. '13]

- $\mathcal{Z}_i^{(m)} = [\mathcal{V}_1, \mathcal{V}_2, \dots, \mathcal{V}_i]$.
- $\text{rank}(R^{(m)}) = \text{rank}(\mathcal{Y}_i^{(m)}) = p + q \quad (B \in \mathbb{R}^{n \times p}, C \in \mathbb{R}^{q \times n}),$

Inexact/Iterative Solution of the SPS

- $\mathcal{Z}_i^{(m)} = [\mathcal{V}_1 + \mathcal{E}_1, \mathcal{V}_2 + \mathcal{E}_2, \dots, \mathcal{V}_i + \mathcal{E}_i],$
- $\text{rank}(R^{(m)}) = (2i + 1) \cdot (p + q),$
- $\mathcal{Y}_i^{(m)}$ can serve as a convergence indicator, but is not the actual residual factor.

Summary



Conclusion

- Explained idea of feedback stabilization for mult-field flow problems.
- Recalled and adapted the concept of inexact Newtons method for the arising projected AREs.
- Discovered a gap in the theory.
- Showed possible computationally efficient criteria to use once this gap has been closed.

Outlook

- Investigate inexact Newton theory to close the gap.
- Extend ideas to the whole nested iteration, i.e. accuracy control for the SPS solvers.
- Implement and test new ideas.

Thank you for your time!



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