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Second Order to Second Order Balancing for Index-1 Vibrational Systems

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Motivation

Adaptive Spindel Support (ASS) with Piezo Actuators

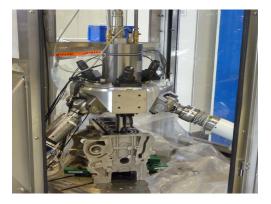


Figure: ASS mounted in Parallel-Kinematic Machine

Source: B. Kranz, Fraunhofer IWU, Dresden, Germany.

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Adaptive Spindel Support (ASS) with Piezo Actuators

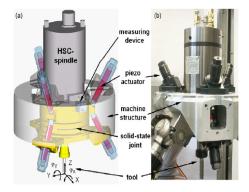


Figure: (a) ASS mounted in (b) Parallel-Kinematic Machine

Source: B. Kranz, Fraunhofer IWU, Dresden, Germany.

Motivation

Adaptive Spindel Support (ASS) with Piezo Actuators

Mathematical Model for Controller Design



$$\mathcal{M}\ddot{x}(t) + \mathcal{D}\dot{x}(t) + \mathcal{K}x(t) = \mathcal{H}u(t)$$

 $y(t) = \mathcal{H}^{T}x(t)$

 ${\cal M}$ mass matrix, ${\cal D}$ damping matrix, ${\cal K}$ stiffness matrix

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Motivation

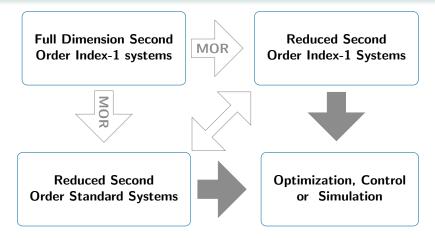
Adaptive Spindel Support (ASS) with Piezo Actuators

Mathematical Model for Controller Design



$$\begin{bmatrix} M_1 & 0\\ 0 & 0 \end{bmatrix} \begin{bmatrix} \ddot{z}(t)\\ \ddot{\varphi}(t) \end{bmatrix} + \begin{bmatrix} D_1 & 0\\ 0 & 0 \end{bmatrix} \begin{bmatrix} \dot{z}(t)\\ \dot{\varphi}(t) \end{bmatrix} + \begin{bmatrix} K_{11} & K_{12}\\ K_{12}^T & K_{22} \end{bmatrix} \begin{bmatrix} z(t)\\ \varphi(t) \end{bmatrix} = \begin{bmatrix} H_1\\ H_2 \end{bmatrix} u(t)$$
$$y(t) = \begin{bmatrix} H_1^T & H_2^T \end{bmatrix} \begin{bmatrix} z(t)\\ \varphi(t) \end{bmatrix}$$







First Order Systems

Given LTI continuous-time system

$$\Sigma: \begin{vmatrix} \dot{x}(t) = Ax(t) + Bu(t), \quad y(t) = Cx(t) + D_au(t) \end{vmatrix}$$

where $x(t) \in \mathbb{R}^n, u(t) \in \mathbb{R}^m, y(t) \in \mathbb{R}^p$ and A, B, C and D_a are matrices

 The realization (A, B, C, D_a), of the system Σ, is called balanced, if the solutions P, Q of the Lyapunov equations (LE)

$$AP + PA^{T} + BB^{T} = 0, \quad \text{[controllability]}$$
$$A^{T}Q + QA + C^{T}C = 0, \quad \text{[observability]}$$

satisfy: $P = Q = \operatorname{diag}(\sigma_1, \dots, \sigma_n)$ where $\sigma_1 \ge \sigma_2 \ge \dots \ge \sigma_n > 0$

• $\{\sigma_1, \ldots, \sigma_n\}$ are the Hankel singular values (HSVs) of Σ



First Order Systems

Given LTI continuous-time system

$$\Sigma: \dot{x}(t) = Ax(t) + Bu(t), \quad y(t) = Cx(t) + D_au(t)$$

• A balanced realization is computed via state space transformation

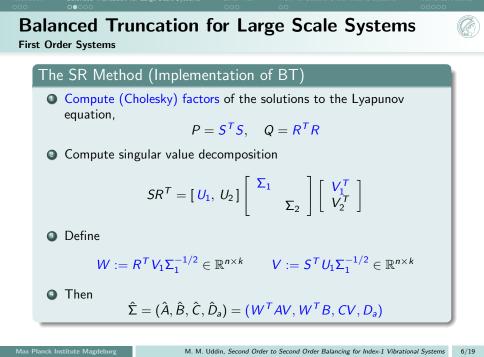
$$\begin{aligned} \mathcal{T} : (A, B, C, D_a) &\mapsto (TAT^{-1}, TB, CT^{-1}, D_a) \\ &= \left(\begin{bmatrix} A_1 & A_2 \\ A_3 & A_4 \end{bmatrix}, \begin{bmatrix} B_1 \\ B_2 \end{bmatrix}, \begin{bmatrix} C_1 & C_2 \end{bmatrix}, D_a \right) \end{aligned}$$

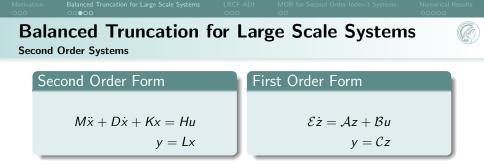
• Form $k \ll n$ dimensional reduced order model:

$$\hat{\Sigma}: \dot{\hat{x}}(t) = \hat{A}\hat{x}(t) + \hat{B}u(t), \quad \hat{y}(t) = \hat{C}\hat{x}(t) + \hat{D}_au(t)$$

where $(\hat{A}, \hat{B}, \hat{C}, \hat{D}_{a}) = (A_{1}, B_{1}, C_{1}, D_{a})$

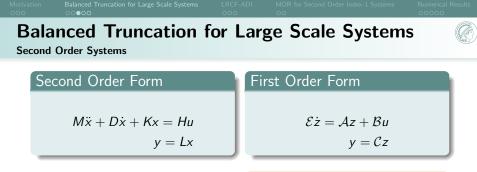
• Such that $\|y - \hat{y}\|_{\infty}$ is small enough





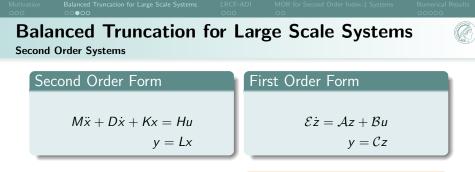
- x displacements
- $z = \left[\dot{x}^T, x^T\right]^T$
- $M, D, K \in \mathbb{R}^{n_1 \times n_1}$ invertible
- J arbitrary but invertible

$$\mathcal{E} = \begin{bmatrix} 0 & J \\ M & D \end{bmatrix}, \quad \mathcal{A} = \begin{bmatrix} J & 0 \\ 0 & -K \end{bmatrix},$$
$$\mathcal{B} = \begin{bmatrix} 0 \\ H \end{bmatrix}, \quad \mathcal{C} = \begin{bmatrix} 0 & L \end{bmatrix}$$



- x displacements
- $z = \left[\dot{x}^T, x^T\right]^T$
- $M, D, K \in \mathbb{R}^{n_1 \times n_1}$ invertible
- **J** = **I** identity matrix

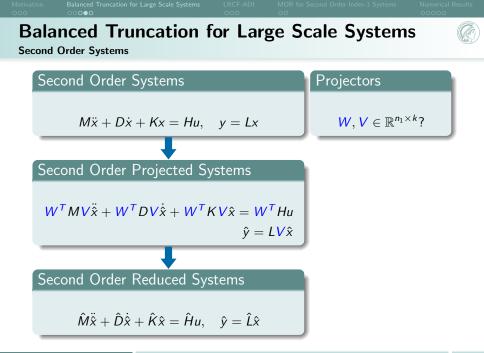
$$\mathcal{E} = \begin{bmatrix} 0 & I \\ M & D \end{bmatrix}, \quad \mathcal{A} = \begin{bmatrix} I & 0 \\ 0 & -K \end{bmatrix},$$
$$\mathcal{B} = \begin{bmatrix} 0 \\ H \end{bmatrix}, \quad \mathcal{C} = \begin{bmatrix} 0 & L \end{bmatrix}$$

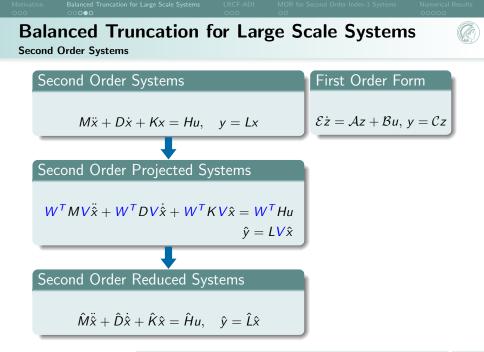


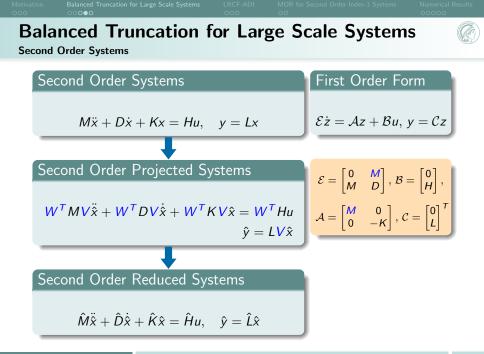
- x displacements
- $z = \left[\dot{x}^T, x^T\right]^T$
- $M, D, K \in \mathbb{R}^{n_1 \times n_1}$ invertible
- J = M for symmetric system

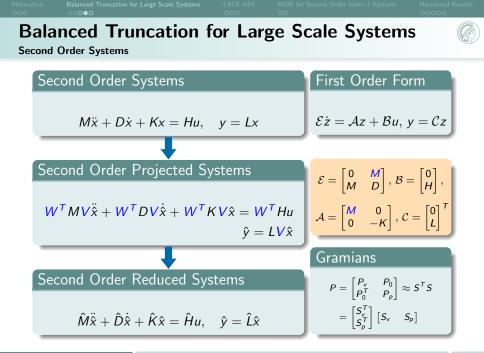
$$\mathcal{E} = \begin{bmatrix} 0 & M \\ M & D \end{bmatrix}, \quad \mathcal{A} = \begin{bmatrix} M & 0 \\ 0 & -K \end{bmatrix},$$
$$\mathcal{B} = \begin{bmatrix} 0 \\ H \end{bmatrix}, \quad \mathcal{C} = \begin{bmatrix} 0 & L \end{bmatrix}$$

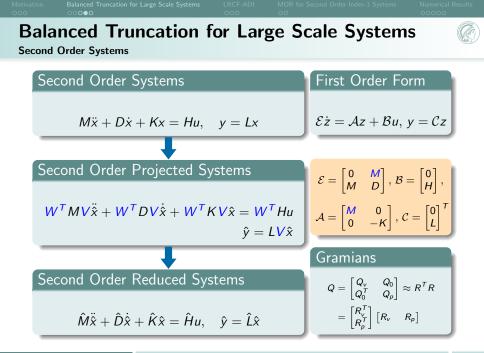
- \bullet First order form is symmetric since ${\cal A}$ and ${\cal E}$ symmetric
- Apply BT methods on first order systems













Second Order Systems

Four Types of Left and Right Projectors

type	SVD	left proj. W	right proj. V
vv	$S_{v}MR_{v}^{T} = U_{vv}\Sigma_{vv}V_{vv}^{T}$	$R_v^T V_{vv,r} \Sigma_{vv,1}^{-\frac{1}{2}}$	$S_v^T U_{vv,1} \Sigma_{vv,1}^{-\frac{1}{2}}$
рр	$S_p M R_p^T = U_{pp} \Sigma_{pp} V_{pp}^T$	$R_p^T V_{pp,r} \Sigma_{pp,r}^{-\frac{1}{2}}$	$S_p^T U_{pp,r} \Sigma_{pp,r}^{-\frac{1}{2}}$
vp	$S_{v}MR_{p}^{T} = U_{vp}\Sigma_{vp}V_{vp}^{T}$	$R_p^T V_{vp,r} \Sigma_{vp,r}^{-\frac{1}{2}}$	$S_v^T U_{vp,r} \Sigma_{vp,r}^{-\frac{1}{2}}$
pv	$S_p M R_v^T = U_{pv} \Sigma_{pv} V_{pv}^T$	$R_v^T V_{pv,r} \Sigma_{pv,r}^{-\frac{1}{2}}$	$S_p^T U_{pv,r} \Sigma_{pv,r}^{-\frac{1}{2}}$

vv = velocity-velocity, pp = position-position,vp = velocity-position, pv = position-velocity,r = first r columns of the respective matrix

Form four types of reduced order model:



Given $FX + XF^T = -GG^T$ $F \in \mathbb{R}^{n \times n}, G \in \mathbb{R}^{n \times p}$

- To solve Controllability LE : F = A and G = B
- To solve Observability LE : $F = A^T$ and $G = C^T$

Task Find $Z \in \mathbb{C}^{n \times nz}$, such that $nz \ll n$ and $X \approx ZZ^H$

Material Parameter Transition for Large Scale Systems LRCF-ADI MOR for Second Order Index 1 Systems Numerical Results Solving Large Lyapunov Equations LRCF-ADI [BENNER/LI/PENZL '08]

Given $FX + XF^T = -GG^T$ $F \in \mathbb{R}^{n \times n}, G \in \mathbb{R}^{n \times p}$

- To solve Controllability LE : F = A and G = B
- To solve Observability LE : $F = A^T$ and $G = C^T$

Task Find $Z \in \mathbb{C}^{n \times nz}$, such that $nz \ll n$ and $X \approx ZZ^H$

Algorithm

$$V_1 = \sqrt{-2 \operatorname{Re}(p_1)} (F + p_1 I)^{-1} G,$$
 $Z_1 = V_1$

$$V_i = \frac{\sqrt{\operatorname{Re}(p_i)}}{\sqrt{\operatorname{Re}(p_{i-1})}} \left[V_{i-1} - (p_i + \overline{p_{i-1}})(F + p_i I)^{-1} V_{i-1} \right], \quad Z_i = [Z_{i-1} V_i]$$

- For certain shift parameters $\{p_1,...,p_l\}\subset \mathbb{C}^-$
- Stop the algorithm if $||FZ_iZ_i^H + Z_iZ_i^HF^T + GG^T||$ is small



Given $FXE^T + EXF^T = -GG^T$ $E, F \in \mathbb{R}^{n \times n}, G \in \mathbb{R}^{n \times p}$

- To solve Controllability LE : F = A and G = B
- To solve Observability LE : $F = A^T$ and $G = C^T$

Task Find $Z \in \mathbb{C}^{n \times nz}$, such that $nz \ll n$ and $X \approx ZZ^H$

Algorithm

$$V_1 = \sqrt{-2 \operatorname{Re}(p_1)} (F + p_1 E)^{-1} G,$$
 $Z_1 = V_1$

$$V_i = \frac{\sqrt{\operatorname{Re}\left(p_i\right)}}{\sqrt{\operatorname{Re}\left(p_{i-1}\right)}} \left[V_{i-1} - (p_i + \overline{p_{i-1}})(F + p_i E)^{-1} E V_{i-1} \right], \quad Z_i = [Z_{i-1} V_i]$$

- For certain shift parameters $\{p_1,...,p_l\}\subset \mathbb{C}^-$
- Stop the algorithm if $||FZ_iZ_i^H E^T + EZ_iZ_i^H F^T + GG^T||$ is small



Index-1 system

$$\begin{bmatrix} \boldsymbol{E}_{11} & \boldsymbol{0} \\ \boldsymbol{0} & \boldsymbol{0} \end{bmatrix} \begin{bmatrix} \dot{x}_1(t) \\ \dot{x}_2(t) \end{bmatrix} = \begin{bmatrix} F_{11} & F_{12} \\ F_{21} & F_{22} \end{bmatrix} \begin{bmatrix} x_1(t) \\ x_2(t) \end{bmatrix} + \begin{bmatrix} B_1 \\ B_2 \end{bmatrix} u(t)$$

Given $\tilde{F}XE_{11}^T + E_{11}X\tilde{F}^T = -\tilde{G}\tilde{G}^T$, $E_{11}, \tilde{F} \in \mathbb{R}^{n \times n}, \tilde{G} \in \mathbb{R}^{n \times p}$

$$\tilde{F} = F_{11} - F_{12}F_{22}^{-1}F_{21}, \quad \tilde{G} = B_1 - F_{12}F_{22}^{-1}B_2$$

Task Find $Z \in \mathbb{C}^{n \times nz}$, such that $nz \ll n$ and $X \approx ZZ^H$

Algorithm

$$\begin{bmatrix} V_1 \\ * \end{bmatrix} = \sqrt{-2\operatorname{Re}(p_1)} \begin{bmatrix} F_{11} + p_1 E_{11} & F_{12} \\ F_{21} & F_{22} \end{bmatrix}^{-1} \begin{bmatrix} B_1 \\ B_2 \end{bmatrix}, \qquad \qquad Z_1 = V_1$$

$$\begin{bmatrix} V_i \\ * \end{bmatrix} = \frac{\sqrt{\operatorname{Re}(p_i)}}{\sqrt{\operatorname{Re}(p_{i-1})}} \begin{bmatrix} V_{i-1} - (p_i + \overline{p_{i-1}}) \begin{bmatrix} F_{11} + p_i E_{11} & F_{12} \\ F_{21} & F_{22} \end{bmatrix}^{-1} \begin{bmatrix} E_{11} V_{i-1} \\ 0 \end{bmatrix} \end{bmatrix}, \qquad Z_i = [Z_{i-1} V_i]$$



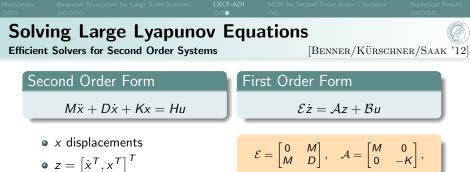
$$\mathsf{Given} \quad \tilde{F}XE_{11}^{\mathsf{T}} + E_{11}X\tilde{F} = -\tilde{G}\tilde{G}^{\mathsf{T}}, \qquad E_{11}, \tilde{F} \in \mathbb{R}^{n \times n}, \tilde{G} \in \mathbb{R}^{n \times p}$$

$$\tilde{F} = F_{11} - F_{12}F_{22}^{-1}F_{21}, \quad \tilde{G} = B_1 - F_{12}F_{22}^{-1}B_2$$

Task Find $Z \in \mathbb{R}^{n \times nz}$, such that $nz \ll n$ and $X \approx ZZ^H$

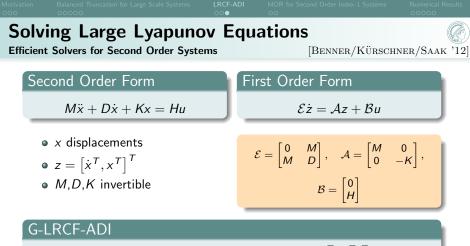
Observation:

$$\begin{array}{ll} \text{If} \quad p_{i+1} = \overline{p_i} \\ V_{i+1} = \overline{V_i} + \beta \text{Im}(V_i) \\ Z_{i+1} = [Z_{i-1}, \sqrt{2}\text{Re}(V_i) + \frac{\beta}{\sqrt{2}}\text{Im}(V_i), \sqrt{\frac{\beta^2}{2} + 2} \text{Im}(V_i)] \\ \text{where} \quad \beta = 2\frac{\text{Re}(p_i)}{\text{Im}(p_i)} \end{array}$$

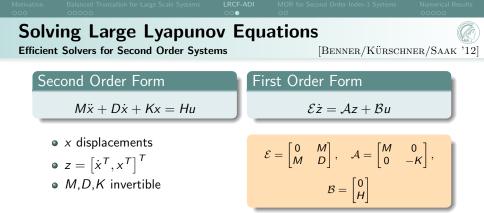


• M,D,K invertible

 $\mathcal{E} = \begin{bmatrix} 0 & M \\ M & D \end{bmatrix}, \quad \mathcal{A} = \begin{bmatrix} M & 0 \\ 0 & -K \end{bmatrix},$ $\mathcal{B} = \begin{bmatrix} 0 \\ H \end{bmatrix}$



main task per step: $(\mathcal{A} + p_i \mathcal{E})x = \mathcal{E}f, \quad x = [x_1^T, x_2^T]^T$



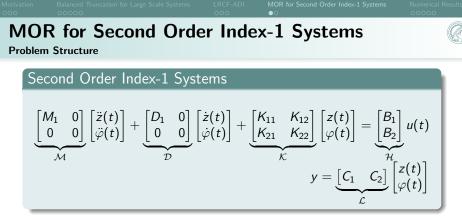
G-LRCF-ADI

main task per step:

$$(\mathcal{A} + p_i \mathcal{E}) x = \mathcal{E}f, \quad x = [x_1^T, x_2^T]^T$$

SO-LRCF-ADI

$$(p_i^2 M - p_i D + K)x_2 = (p_i M - D)f_2 - Mf_1, \qquad x_1 = f_2 - p_i x_2$$



where $\mathcal{M}, \mathcal{D}, \mathcal{K} \in \mathbb{R}^{n_1 \times n_1}$, $\mathcal{H} \in \mathbb{R}^{n_1 \times p}$ and $\mathcal{L} \in \mathbb{R}^{m \times n_1}$

Properties

- All matrices are sparse
- \mathcal{M} and \mathcal{D} are singular, K_{22} is invertible

$$\underbrace{\begin{array}{c} \text{MOR for Second Order Index 1 Systems}_{QOO} \\ \hline \textbf{MOR for Second Order Index 1 System$$

Problem Structure

$$\widehat{M_{1}} \stackrel{?}{Z}(t) + \widehat{D_{1}} \stackrel{?}{Z}(t) + (\widehat{K_{11}} - \widehat{K_{12}}K_{22}^{-1}\widehat{K_{21}})\widehat{z}(t) = (\widehat{B}_{1} - \widehat{K_{12}}K_{22}^{-1}B_{2})u(t)$$

$$\widehat{W}_{1} \stackrel{?}{Z}(t) + \widehat{D}_{1} \stackrel{?}{Z}(t) + (\widehat{K_{11}} - \widehat{K_{12}}K_{22}^{-1}\widehat{K_{21}})\widehat{z}(t) = (\widehat{B}_{1} - \widehat{K_{12}}K_{22}^{-1}B_{2})u(t)$$

$$\widehat{W}_{1} \stackrel{?}{Z}(t) + \widehat{D}_{1} \stackrel{?}{Z}(t) + (\widehat{K_{11}} - \widehat{K_{12}}K_{22}^{-1}\widehat{K_{21}})\widehat{z}(t) = (\widehat{B}_{1} - \widehat{K_{12}}K_{22}^{-1}B_{2})u(t)$$

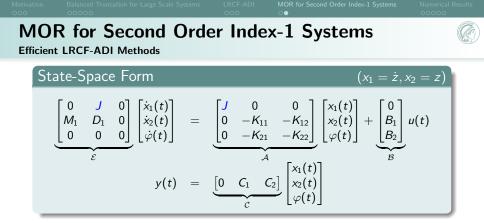
$$\widehat{Y} = (\widehat{C}_{1} - C_{2}K_{22}^{-1}\widehat{K_{21}})\widehat{z}(t) + (\widehat{C}_{2}K_{22}^{-1}B_{2})u(t)$$

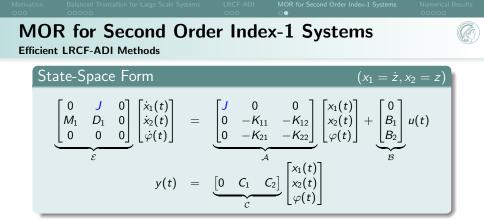
$$\hat{M}_1 = W^T M_1 V, \quad \hat{D}_1 = W^T D_1 V, \quad \hat{K}_{11} = W^T K_{11} V, \quad \hat{K}_{12} = W^T K_{12} \hat{K}_{21} = K_{21} V, \quad \hat{B}_1 = W^T B_1, \quad \hat{C}_1 = C_1 V$$

$$(Married a) = (Married a) (M$$

$$\underbrace{\begin{bmatrix} \hat{n}_{1} & 0 \\ 0 & 0 \end{bmatrix}}_{\hat{\mathcal{M}}} \begin{bmatrix} \hat{\varphi}(t) \end{bmatrix} + \underbrace{\begin{bmatrix} 0 & 1 \\ 0 & 0 \end{bmatrix}}_{\hat{\mathcal{D}}} \begin{bmatrix} \hat{\varphi}(t) \end{bmatrix} + \underbrace{\begin{bmatrix} \hat{\kappa}_{1} & \kappa_{2} \\ \hat{\kappa} \end{bmatrix}}_{\hat{\mathcal{K}}} \begin{bmatrix} \varphi(t) \end{bmatrix} = \underbrace{\begin{bmatrix} B_{1} \\ B_{2} \end{bmatrix}}_{\hat{\mathcal{L}}} \begin{bmatrix} u(t) \\ \varphi(t) \end{bmatrix}$$
$$y = \underbrace{\begin{bmatrix} \hat{C}_{1} & C_{2} \end{bmatrix}}_{\hat{\mathcal{L}}} \begin{bmatrix} \hat{z}(t) \\ \varphi(t) \end{bmatrix}$$

$$(A) \\ (A) \\ (A)$$





Advantages

•
$$B_1 = C_1^T$$
, $B_2 = C_2^T \Rightarrow \mathcal{B} = \mathcal{C}^T$

• $J = M_1 \Rightarrow \mathcal{E}, \mathcal{A}$ symmetric

 \Rightarrow System symmetric \Rightarrow Lyapunov equations coincide



Linear System Inside the ADI

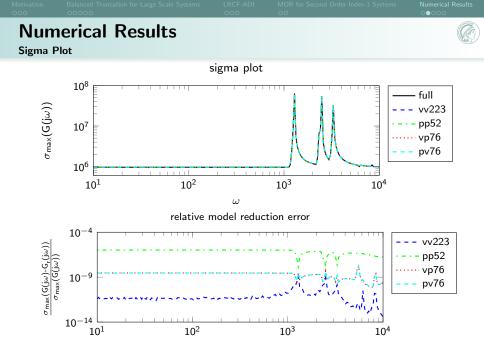
$$\begin{bmatrix} M_1 & \mu_1 M_1 & 0\\ \mu_1 M_1 & \mu_1 (D_1 - K_{11}) & -K_{12}\\ 0 & -K_{21} & -K_{22} \end{bmatrix} \begin{bmatrix} x_1^{(i)}\\ x_2^{(i)}\\ \Lambda \end{bmatrix} = \begin{bmatrix} 0\\ f_1\\ f_2 \end{bmatrix}$$

• Solve
$$\begin{bmatrix} \mu_1^2 M_1 - \mu_1 D_1 + K_{11} & K_{12} \\ K_{21} & K_{22} \end{bmatrix} \begin{bmatrix} x_{2}^{(i)} \\ \Lambda \end{bmatrix} = \begin{bmatrix} f_1 \\ f_2 \end{bmatrix}$$
 for $x_2^{(i)}$
• If $i = 1$, $f_1 = -B_1$, $f_2 = -B_2$ and $x_1^{(1)} = -\mu_1 x_2^{(1)}$
• Otherwise, $f_1 = (p_i V_{i-1}^{(2)} - V_{i-1}^{(1)})M_1 + D_1 V_{i-1}^{(2)}$, $f_2 = 0$ and $x_1^{(i)} = -p_i x_2^{(i)} + V_{i-1}^{(2)}$
• $V_{i-1} = \begin{bmatrix} V_{i-1}^{(1)} \\ V_{i-1}^{(2)} \end{bmatrix}$ (see ADI methods)



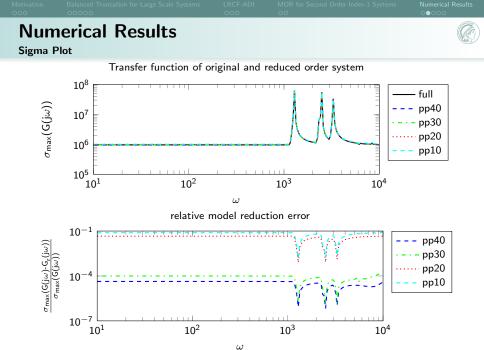
- Dimension of full model: 290137
- ADI optimal shift parameters: 40
- ADI iteration steps 400 to compute $Z \in \mathbb{R}^{n \times nz}$
- Number of inputs/outputs: 9
- Tolerance for ROM: 10^{-3}
- Dimension of reduced order models in different balancing levels:

different types	ROM dimension
velocity-velocity (vv)	223
position-position (pp)	52
velocity-position (vp)	76
position-velocity (pv)	76

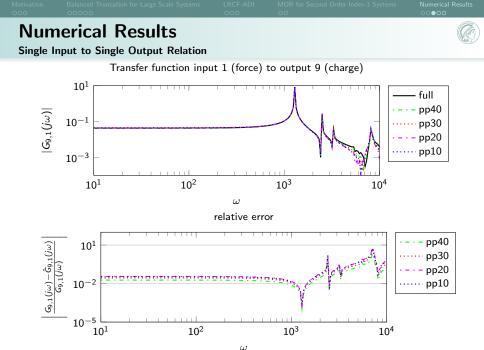


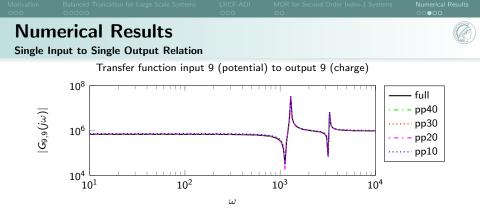
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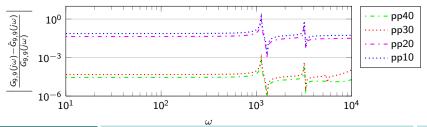


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relative error



		Numerical Results ○○○●○

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Conclusion and Outlook

Overview

- Second order to second order MOR techniques are shown for second order index-1 systems, and applied to ASS model
- The accuracy of the method is demonstrated by a frequency domain error analysis
- Even very low order surrogate models (10dof) preserve the main features of the transfer behavior of the full (290137dof) FEM model
- They are expected to perform well in controller design
- Our approach performs well on any computer that can solve the finite element model

Future Work

• Implicit handling of higher index, e.g., structural dynamics with holonomic constraints

Conclusion and Outlook



Overview

- Second order to second order MOR technia shown for second
- d by a frequency domain
- The accuracy of the method is demonstrated by a error analysis
 Even very low order surrogate provide (10dof) present features of the transfer behavior the full (200127). (10dof) preserve the main the full (290137dof) FEM model
 - well in controller design
- VOL Our approach perforp on any computer that can solve the finite element more thank

Future Work

 Implicit handling of higher index, e.g., structural dynamics with holonomic constraints

			Numerical Results ○○○○●
Refe	erences		

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